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Implementation of the Bitumen Performance Grading System in Estonia

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Outline

- **How US has reached to currently valid Superpave standards.**
- **On-going research in bitumen and asphalt mixtures.**
 - **What should be the bitumen properties in pavements.**
 - **What should be the composition of asphalt mixtures to ensure a 20-30 year long lifespan of pavements.**
- **Comments on study of bitumen sources used in Estonia**
- **Concluding Remarks**

Bitumen Standards – USA Overview

- **1930's – Pen** grading
- **1960's – Viscosity** grading
- **1993 - Superpave** testing system proposed
- **1996- PG** grading implemented
- **2000- PG (Plus)** – more complex
- **2002- Damage Resistance** Testing – NCHRP 9-10:
 - 2008 (MSCR)
 - 2011 (BBS)
 - 2013 (LAS)
 - 2014 (SENB, BYET, DSR-ER)

Common Targets for Bitumen Specifications - Performance Based Grading

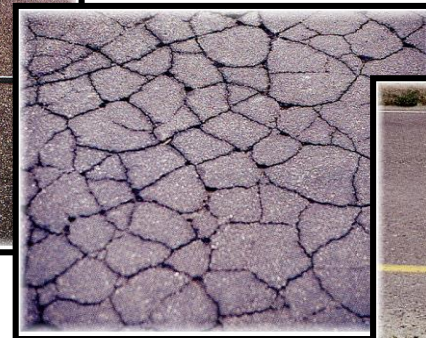
- **Constructability**



- **Performance**



Rutting



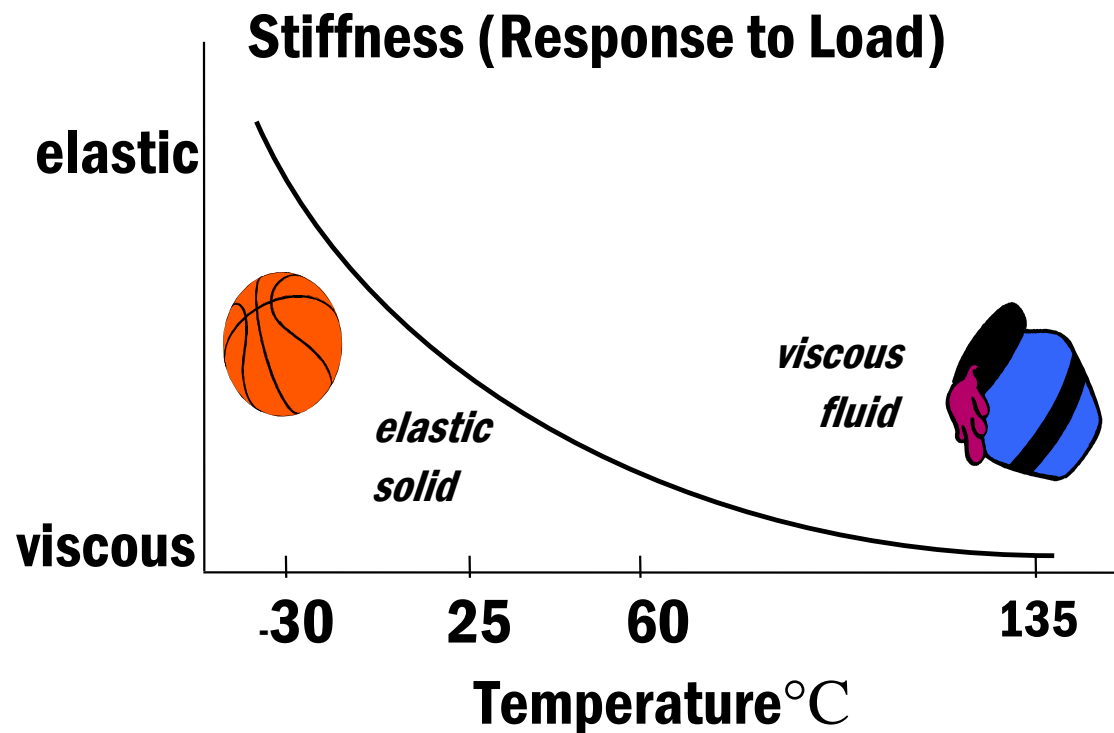
Fatigue Cracking



Thermal Cracking

- **Durability**

Properties of Asphalt Binders

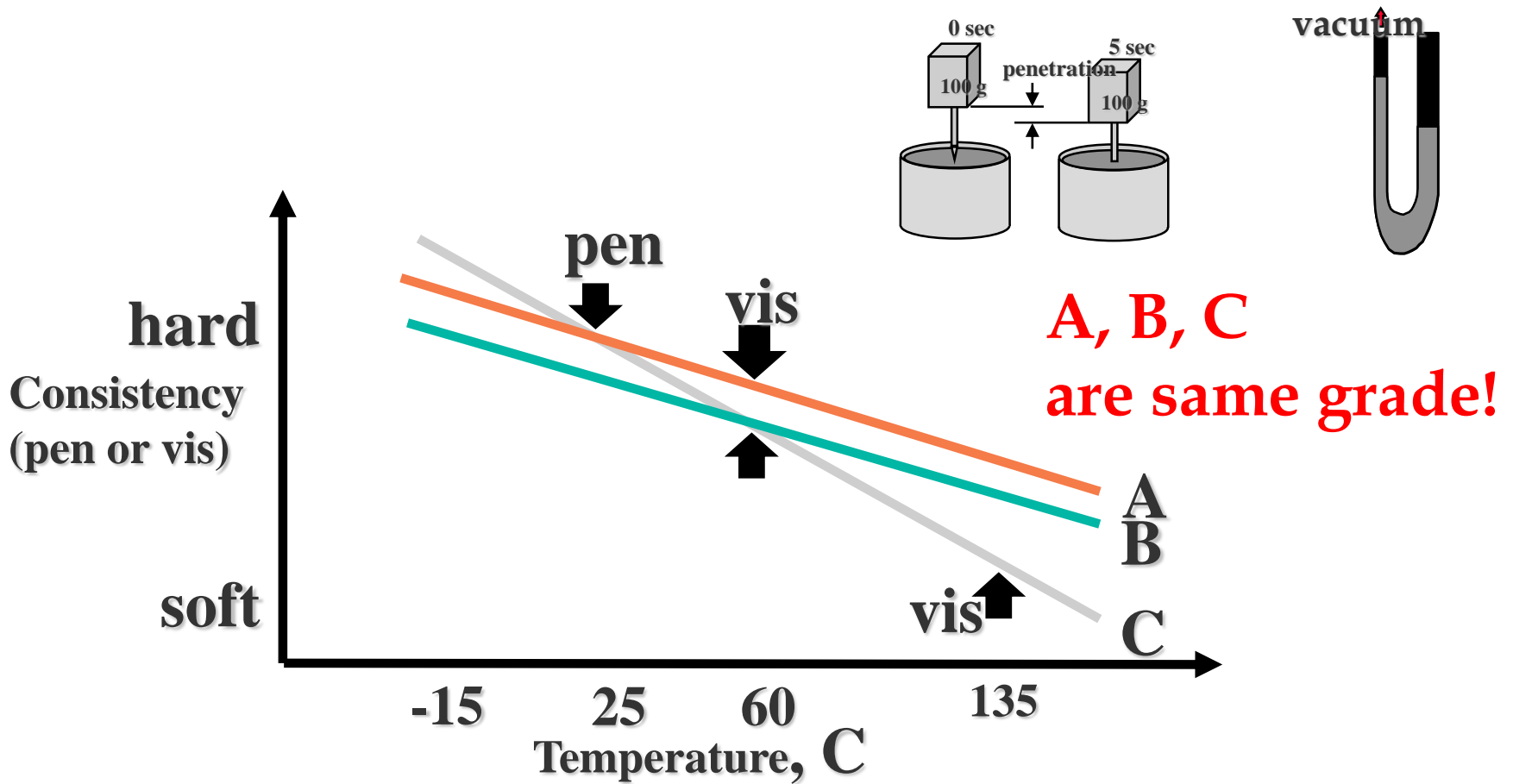


Cold climates ==> use soft-grade asphalts

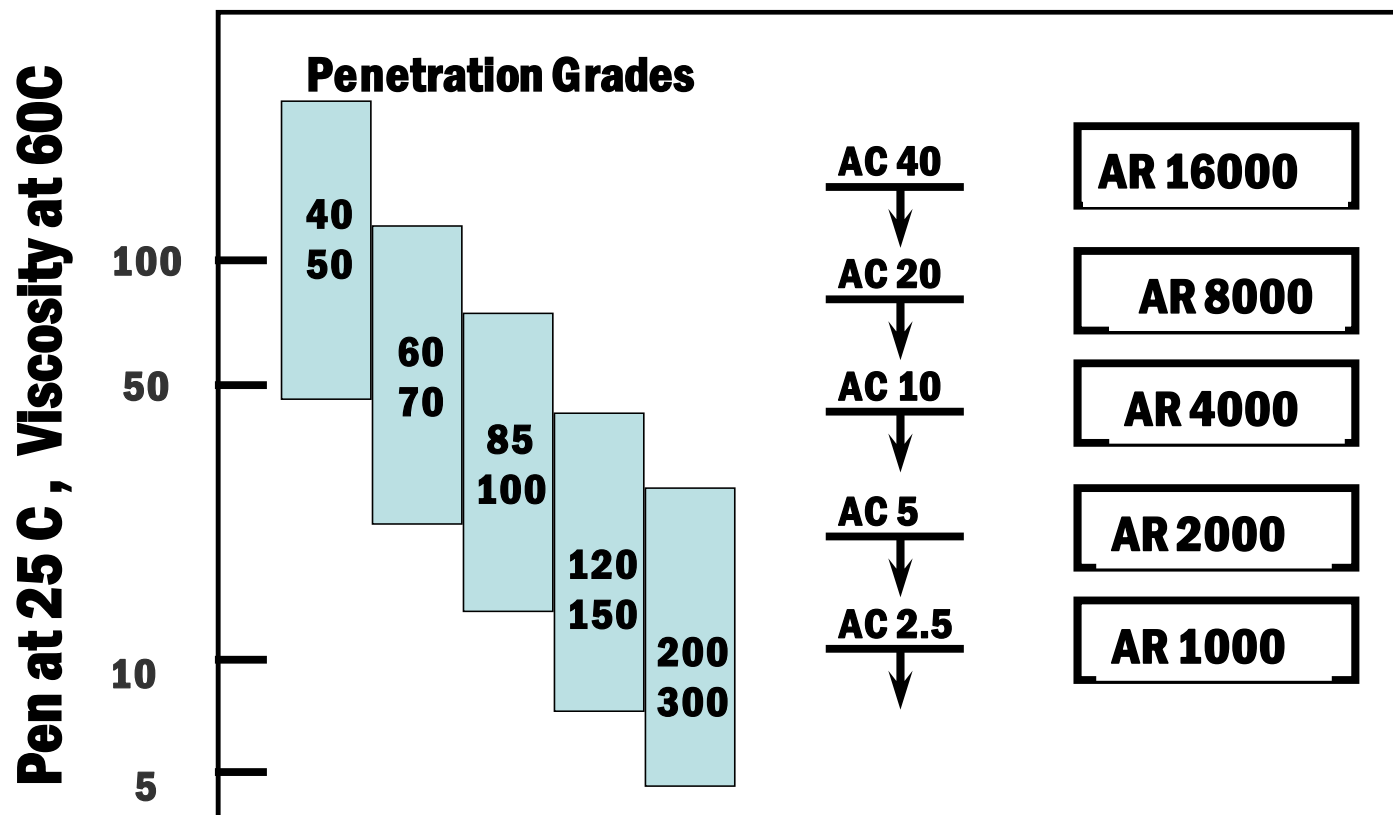
Warm climates ==> use hard-grade asphalts

- Asphalt binder is a **temperature-susceptible viscoelastic material**
- **Change in stiffness with temperature dictates in-service response to loading.**
- **High strain/stress behavior dictates performance.**

Historical Specifications – Pen & Vis



Conventional Asphalt Grades- 1930s - 1990s



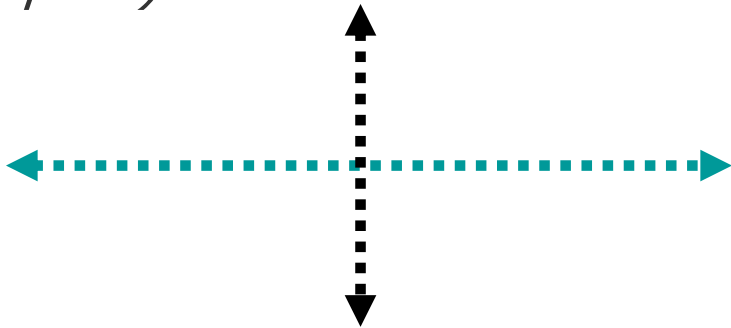
Performance Grading Should:

- Include **measures describing stress-strain relationships** under field climate and loading.
- Consider pavement conditions:
 - **Temperature (pavement)**
 - **Traffic speed and volume,**
 - **Pavement structure, and aging.**
- Include **acceptance limits** derived from factual field performance/experience.

Asphalt Behavior – Visco-elastic

Lower Temp

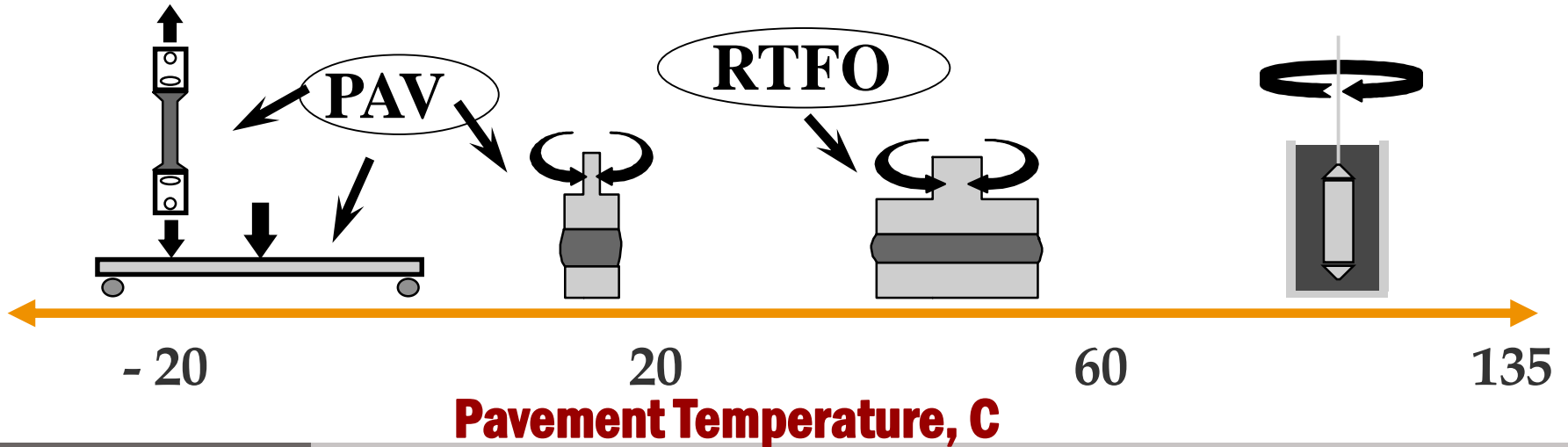
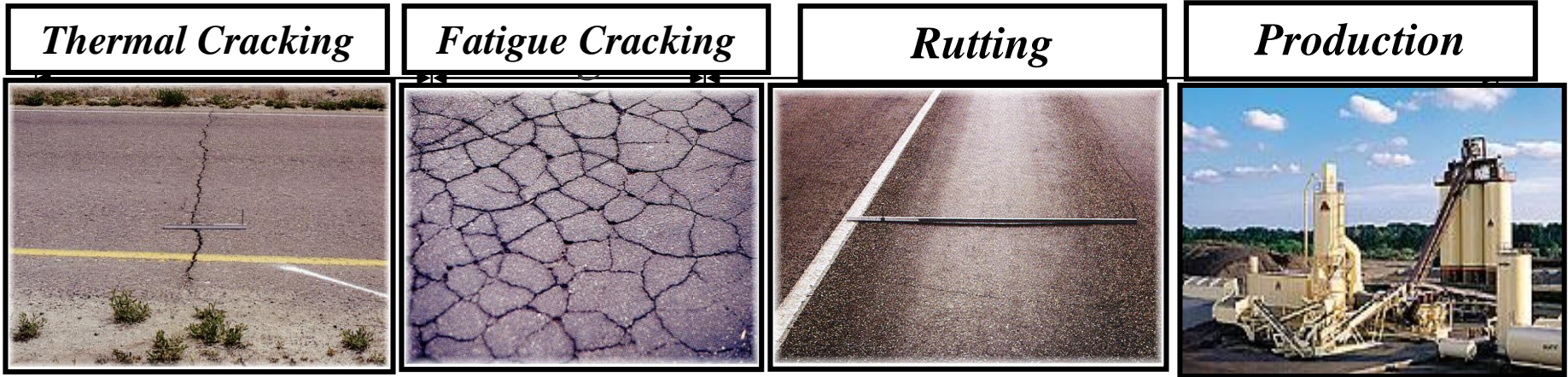
*Shorter loading time
(High Traffic Speed)*



Higher Temp

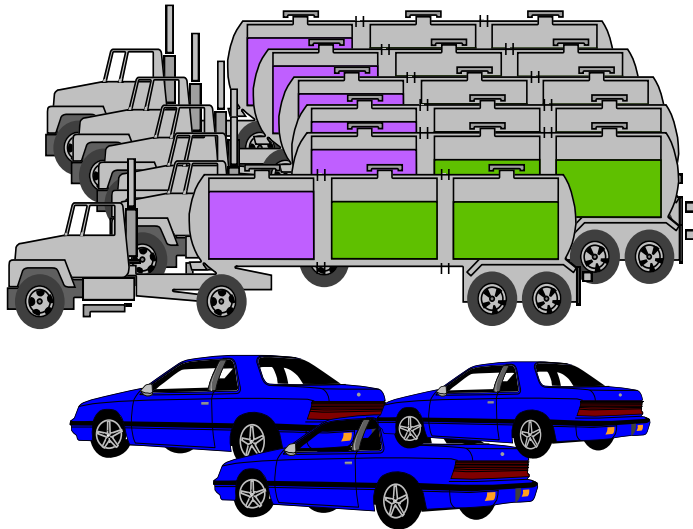
*Longer loading time
Slower Traffic Speed*

Fundamental Rheology Tests – PG System



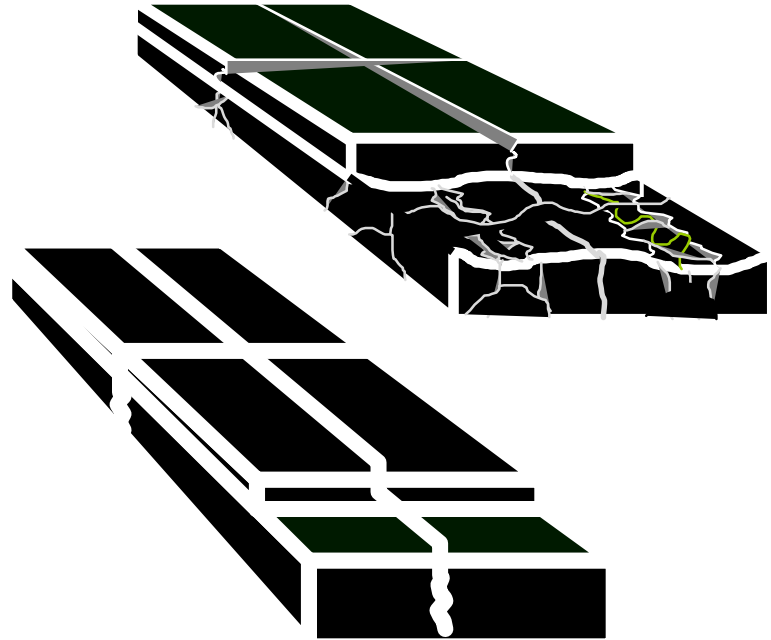
Important Considerations: Traffic and Pavement Structure

Effect of traffic Volume & Speed



ESALS and Speed limits !

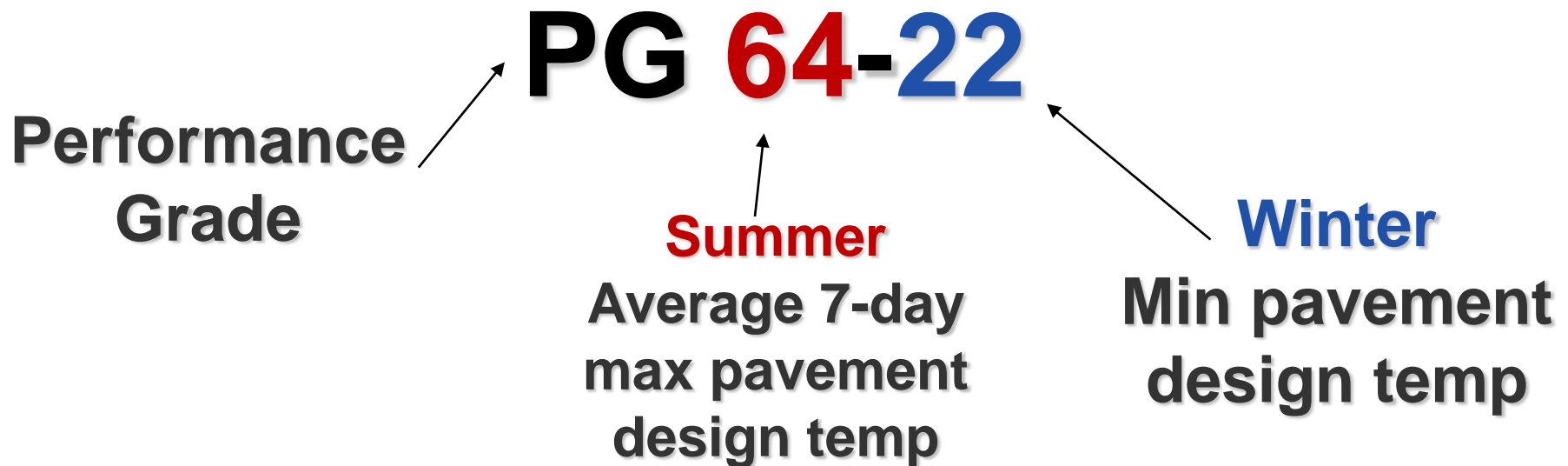
Pavement Damage



Weak vs. Strong base!

Current Performance Grading System- PG

- 1. Climate*
- 2. Traffic conditions- Indirectly*
- 3. Reliability*



PG Grades and Binder Modification

		High Temperature, °C				
		52	58	64	70	76
Low Temperature, °C	-16	52-16	58-16	64-16	70-16	76-16
	-22	52-22	58-22	64-22	70-22	76-22
	-28	52-28	58-28	64-28	70-28	76-28
	-34	52-34	58-34	64-34	70-34	76-34
	-40	52-40	58-40	64-40	70-40	76-40

= Crude Oil
 = High Quality Crude Oil
 = Modifier Required

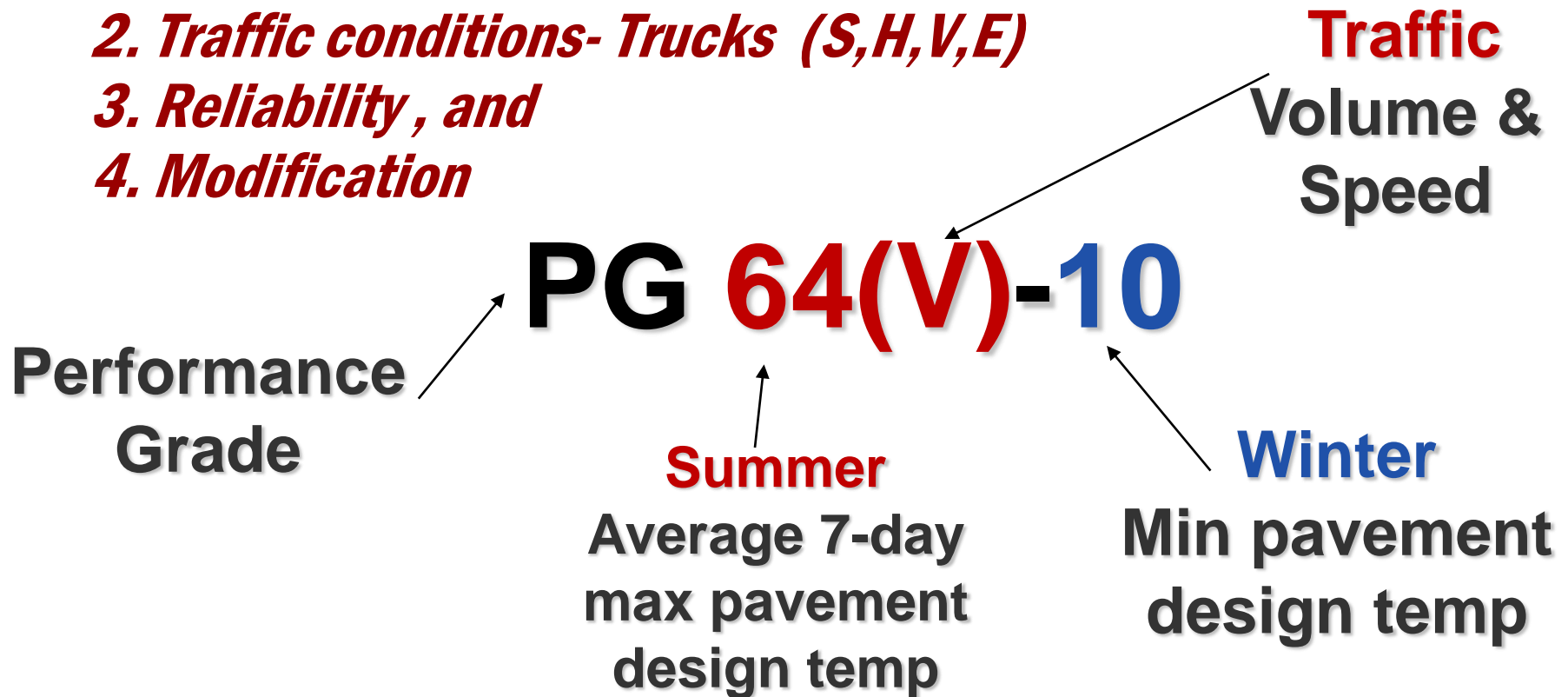
Reasons for Modified Binders

1. Extreme Climates (i.e. AZ or WI)
2. Slow/Standing Traffic
3. Poor subgrade Support

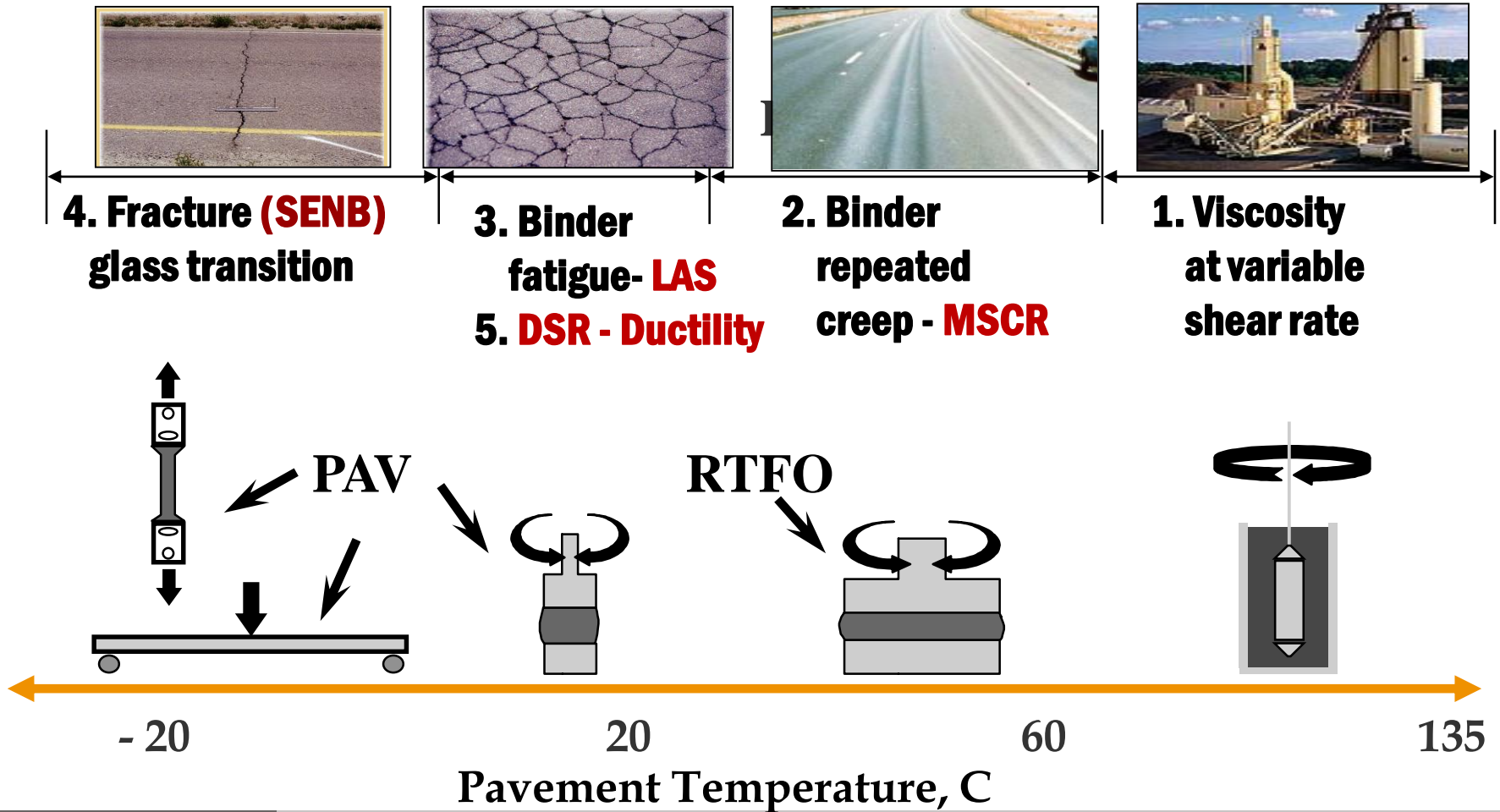
<http://www.pavementinteractive.org/article/superpave-performance-grading/>

The New Grading System- MP19 – PG xx(z)-yy

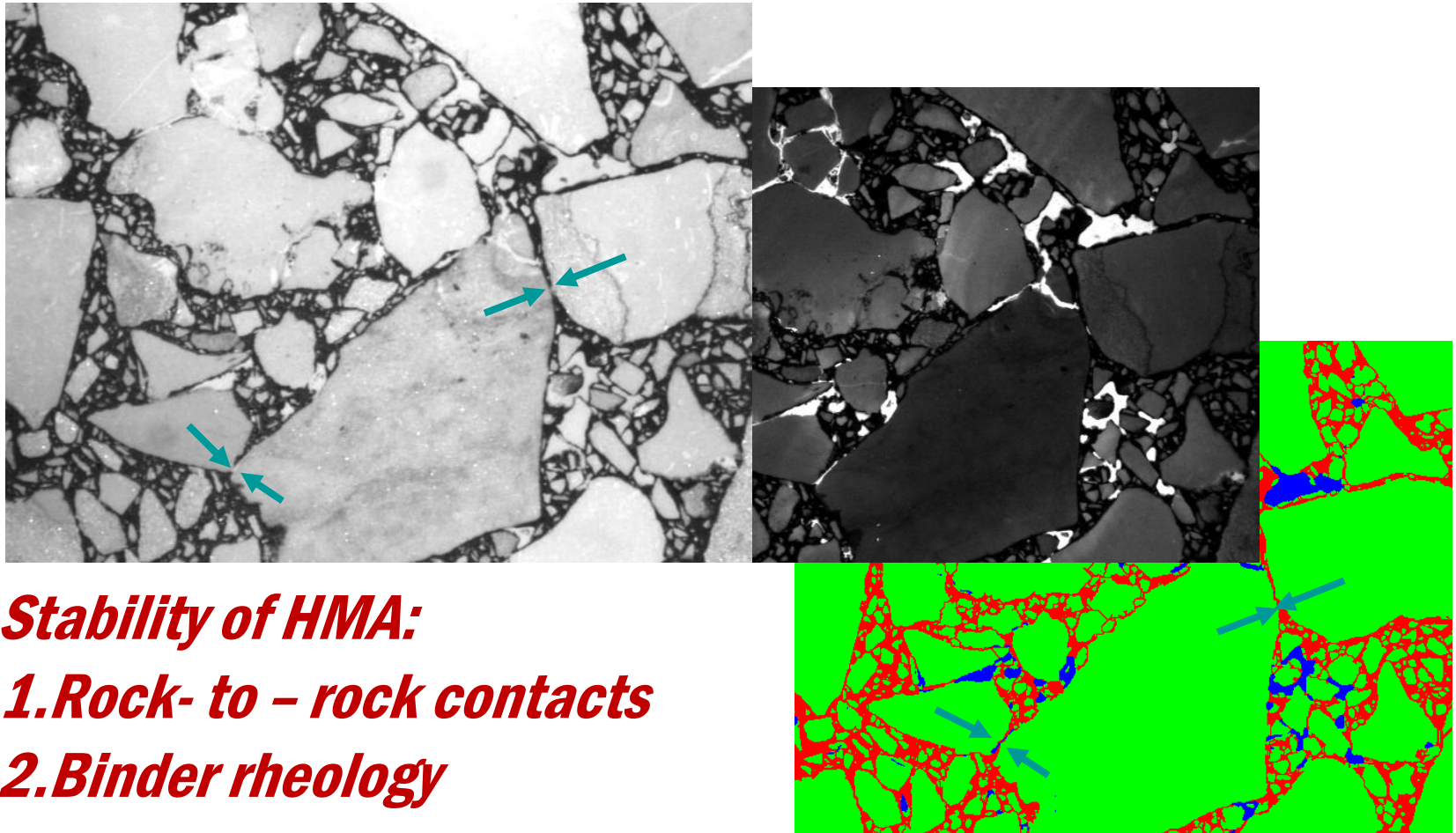
- 1. Climate: xx-yy*
- 2. Traffic conditions- Trucks (S,H,V,E)*
- 3. Reliability, and*
- 4. Modification*



New / advanced testing needed for modified asphalts



HMA Basics: Rocks + Asphalt + Air Voids

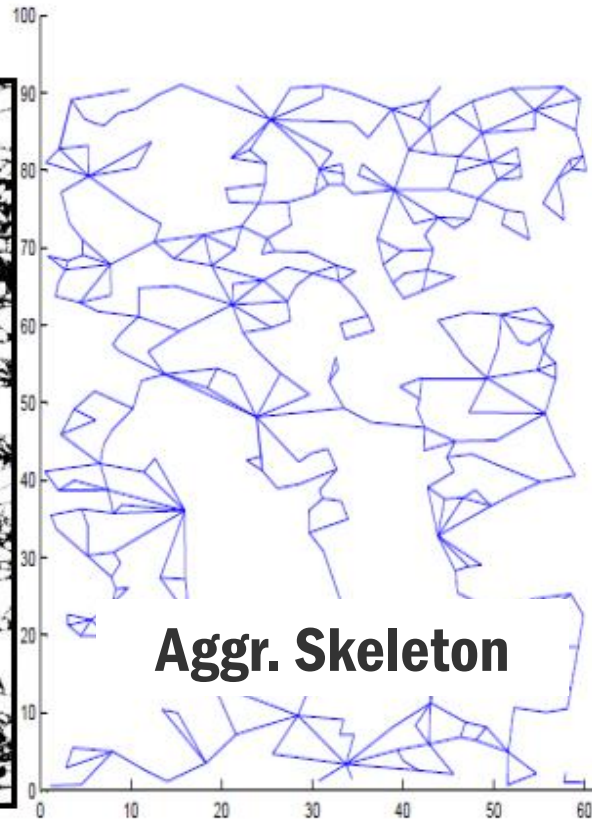


Stability of HMA:
1. Rock- to – rock contacts
2. Binder rheology

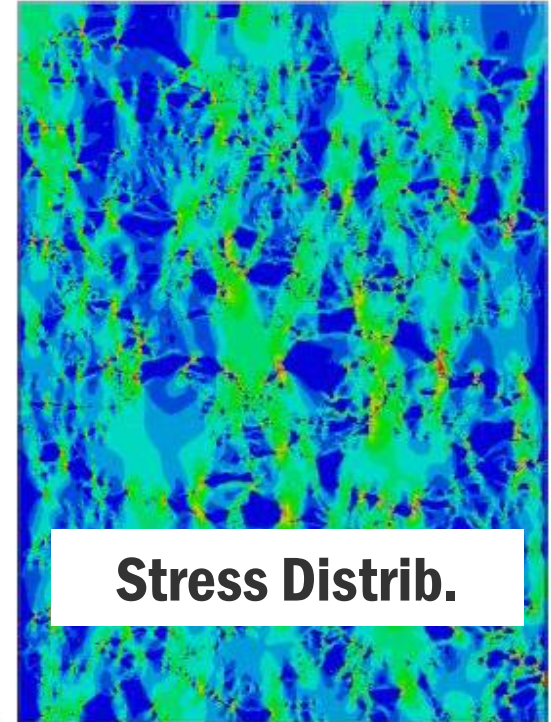
Aggregate Structure in Mix is very Important



Digital Image



Aggr. Skeleton

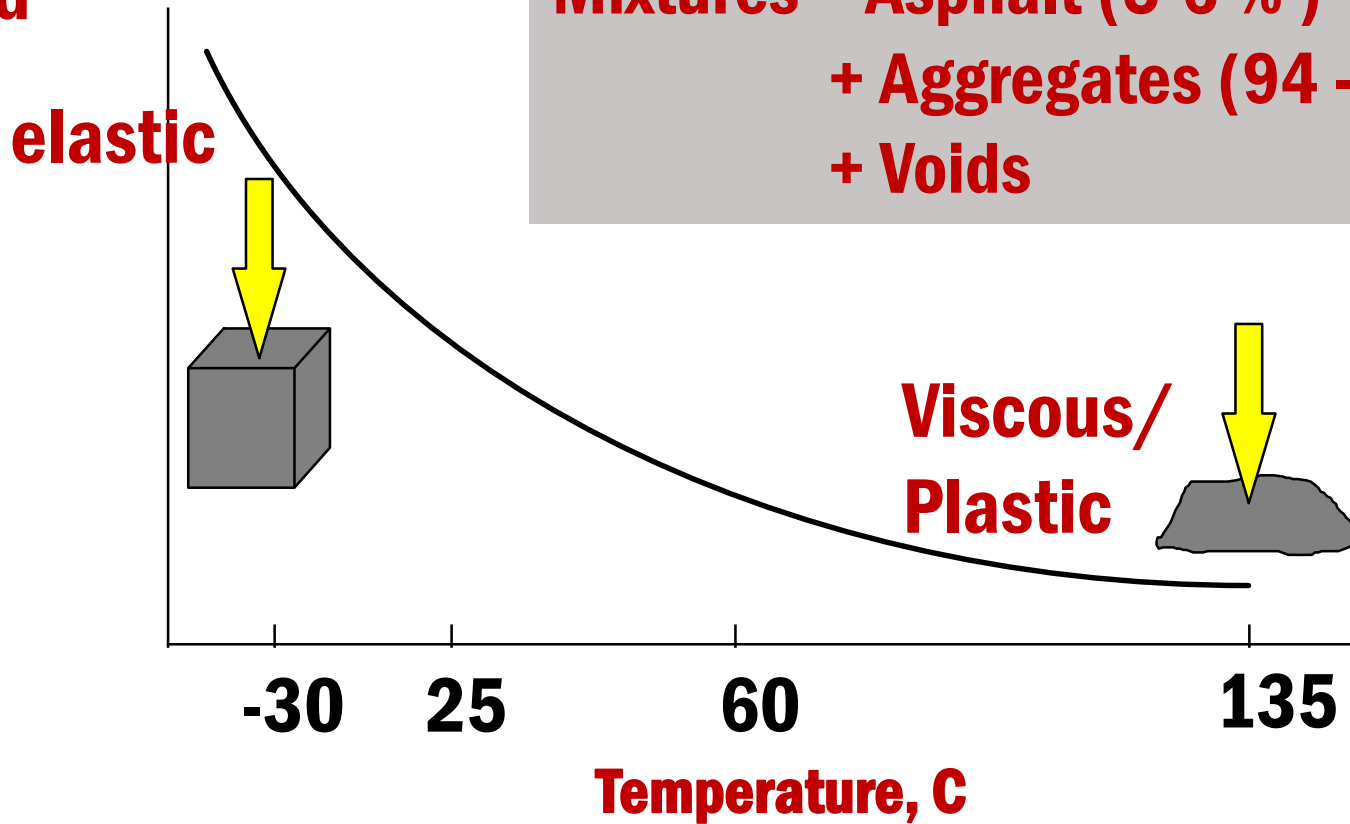


Stress Distrib.

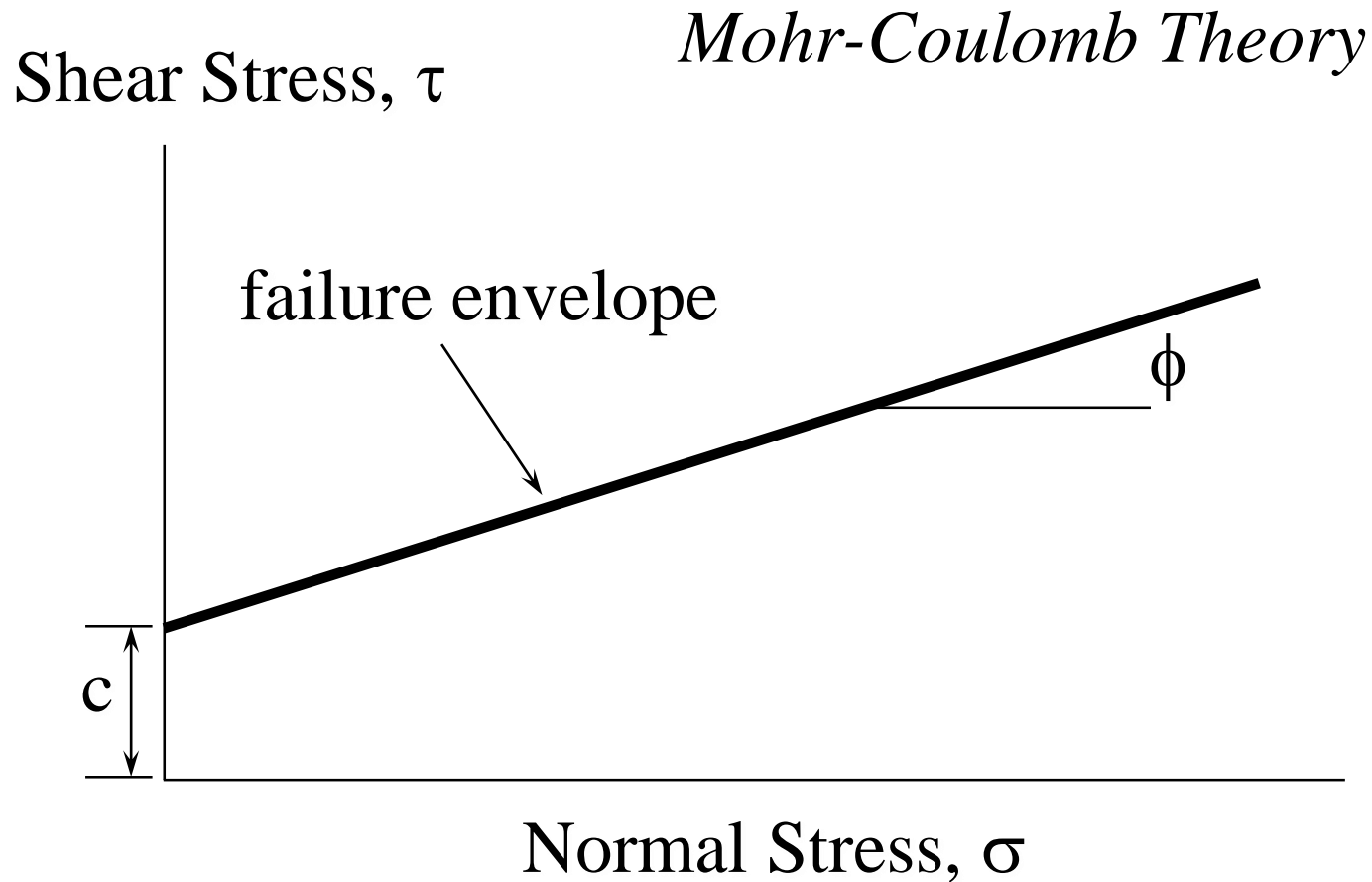
How can we measure it? Can we specify it? What factors control it?

Mixture Response to Load and Climate

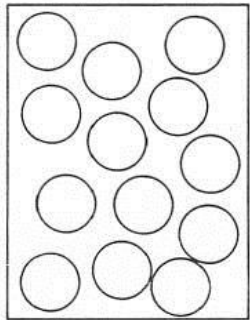
Stiffness Response to Load



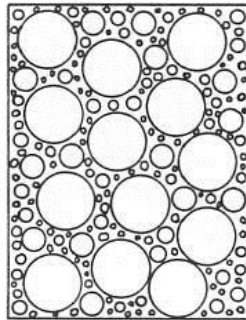
Shearing Behavior of Aggregate



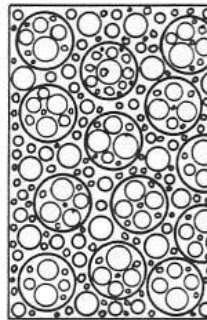
Aggregate gradation and voids between aggregates – Packing



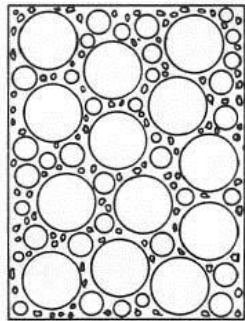
(a)



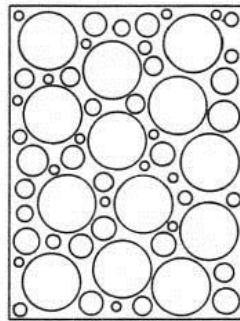
(b)



(c)



(d)

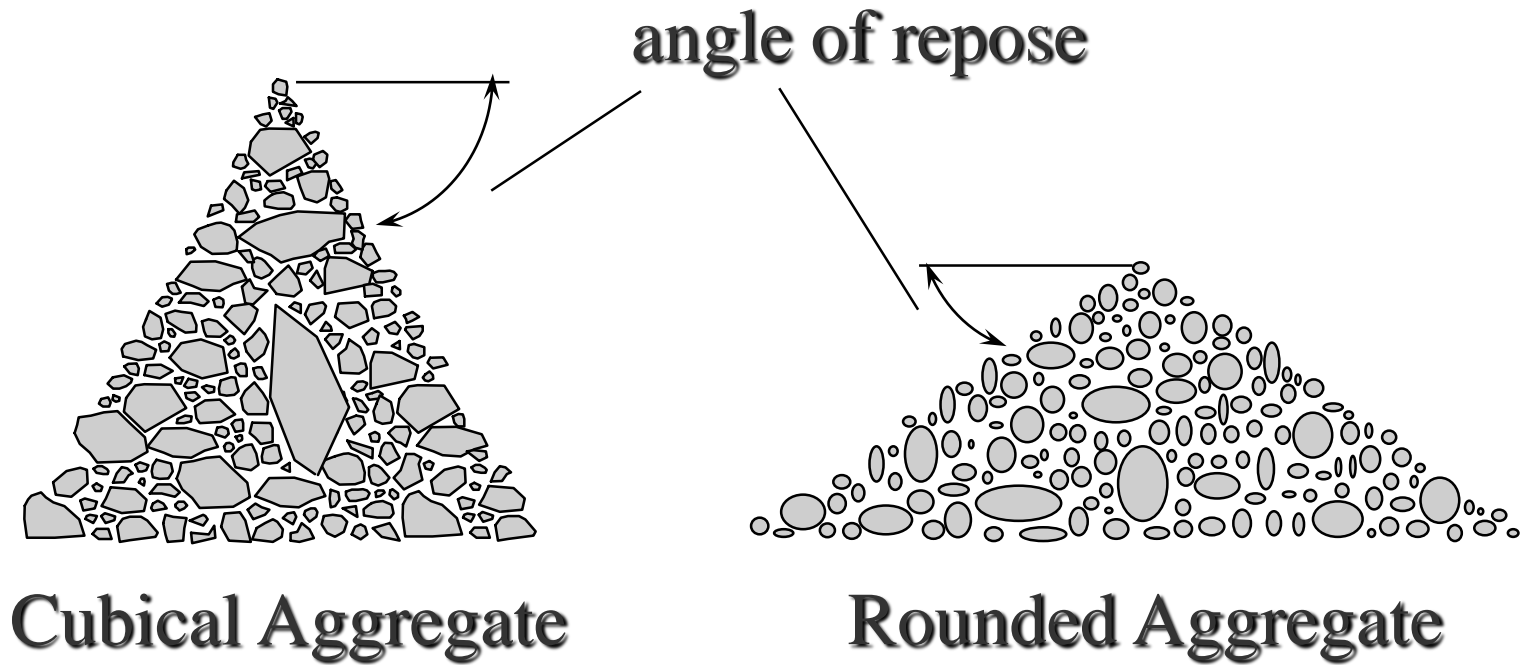


(e)

Voids will

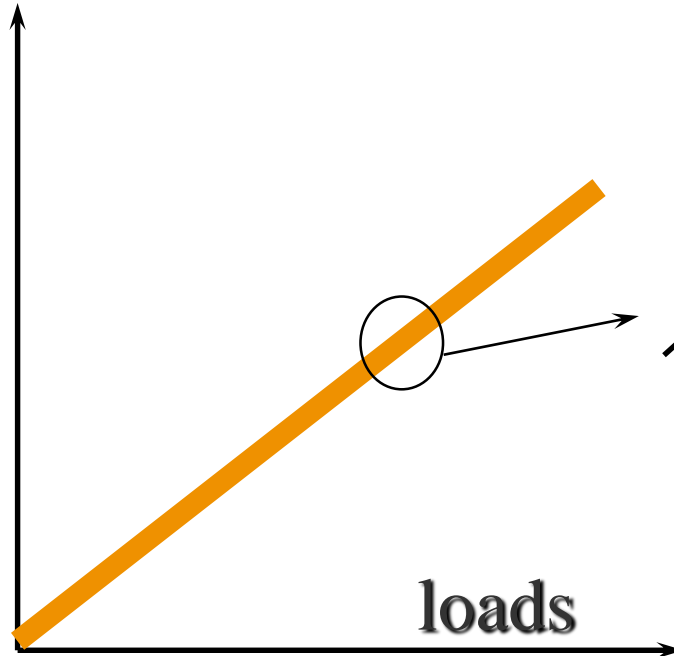
1. reduce stiffness (modulus)
2. Increase amount of cement / asphalt required (cost)
3. Increase permeability
4. Affect workability

Shearing Behavior of Aggregate



Deformation in Asphalt Layers

deformation



Elastic/ Delayed elastic

Viscous/plastic

Mix Design and Testing Progress

- **Earlier methods**
 - Marshall Mix Design, Hveem Mix Design
- **In the 1970-80's**
 - Texas Gyrotory Mix Design, other Empirical Strength Testing
- **In the 1990's**
 - Superpave Gyrotory and Aggregate testing system (1994)
- **In 2000**
 - Hamburg, APA, SPT
- **In 2010s**
 - AMPT, Bailey Method, Imaging

Superpave Mixture Performance Tests

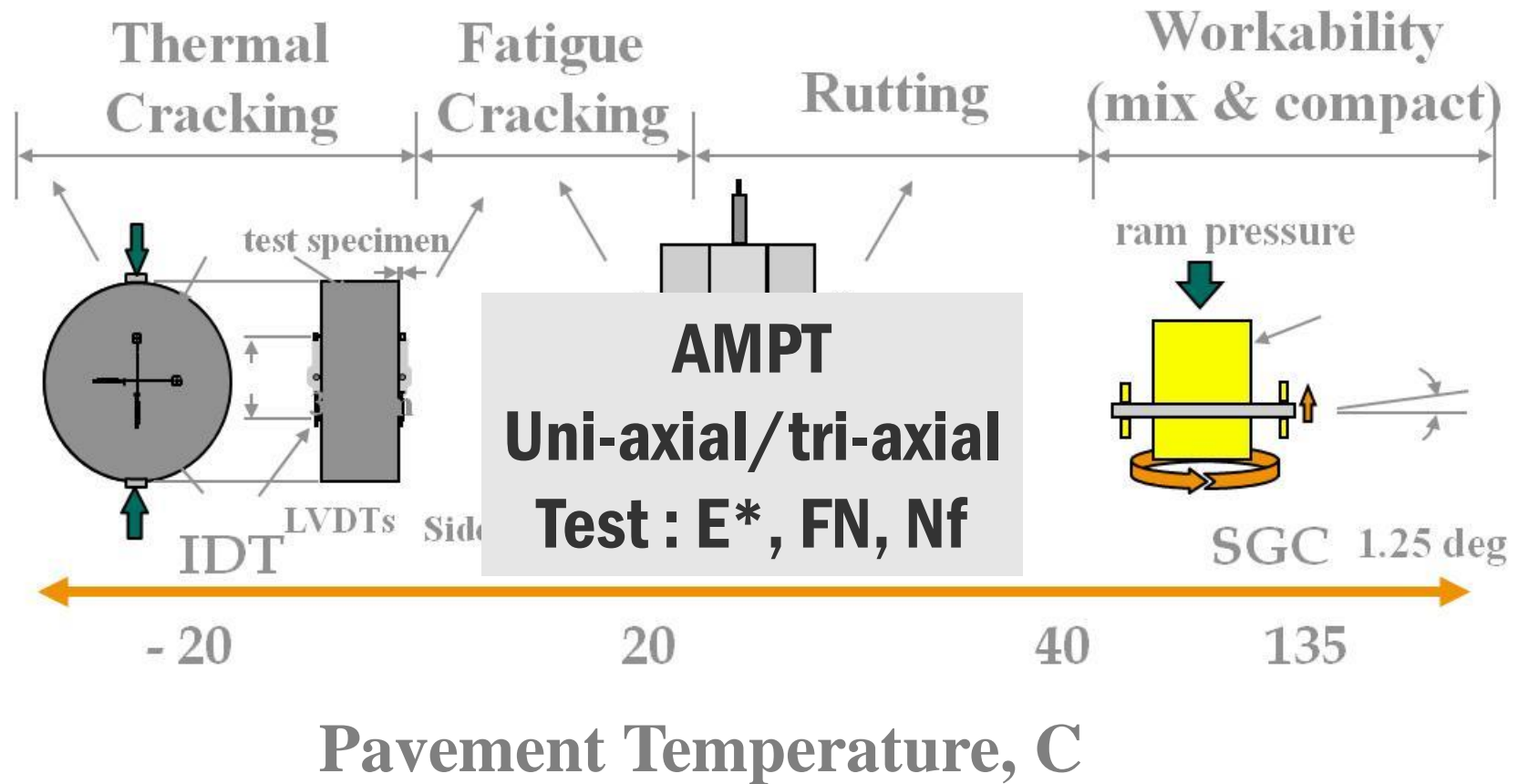


TABLE 460-2 MIXTURE REQUIREMENTS

Mixture type	E - 0.3	E - 1	E - 3	E - 10	E - 30	E - 30x	SMA
ESALs x 10 ⁶ (20 yr design life)	< 0.3	0.3 - < 1	1 - < 3	3 - < 10	10 - < 30	≥ 30	—
LA Wear (AASHTO T 98)							
100 revolutions(max % loss)	13	13	13	13	13	13	13
500 revolutions(max % loss)	50	50	45	45	45	45	45
Soundness (AASHTO T 104) (sodium sulfate, max % loss)	12	12	12	12	12	12	12
Freeze/Thaw (AASHTO T 103) (specified counties, max % loss)	18	18	18	18	18	18	18
Fractured Faces (ASTM 5821) (one face/2 face, % by count)	60 / —	65 / —	75 / 60	85 / 80	98 / 90	100/100	100/90
Thin or Elongated (ASTM D4791) (max %, by weight)	5 (5:1 ratio)	5 (5:1 ratio)	5 (5:1 ratio)	5 (5:1 ratio)	5 (5:1 ratio)	5 (5:1 ratio)	20 (3:1ratio)
Fine Aggregate Angularity (AASHTO T304, method A, min)	40	40	43	45	45	45	45
Sand Equivalency (AASHTO T 176, min)	40	40	40	45	45	50	50
Gyratory Compaction							
Gyrations for N _{ini}	6	7	7	8	8	9	8
Gyrations for N _{des}	40	60	75	100	100	125	100
Gyrations for N _{max}	60	75	115	160	160	205	160
Air Voids, %V _a (%G _{mm} @ N _{des})	4.0 (96.0)	4.0 (96.0)	4.0 (96.0)	4.0 (96.0)	4.0 (96.0)	4.0 (96.0)	4.0 (96.0)
% G _{mm} @ N _{ini}	≤ 91.5 ^[1]	≤ 90.5 ^[1]	≤ 89.0 ^[1]	≤ 89.0	≤ 89.0	≤ 89.0	—
% G _{mm} @ N _{max}	≤ 98.0	≤ 98.0	≤ 98.0	≤ 98.0	≤ 98.0	≤ 98.0	—
Dust to Binder Ratio ^[2] (% passing 0.075/P _{we})	0.6 - 1.2	0.6 - 1.2	0.6 - 1.2	0.6 - 1.2	0.6 - 1.2	0.6 - 1.2	1.2 - 2.0
Voids filled with Binder (VFB or VFA, %)	70 - 80 [4] [6]	65 - 78 [4]	65 - 75 [4]	65 - 75 [3] [4]	65 - 75 [3] [4]	65 - 75 [3] [4]	70 - 80
Tensile Strength Ratio (TSR) (ASTM 4867)							
no antistripping additive	0.70	0.70	0.70	0.70	0.70	0.70	0.70
with antistripping additive	0.75	0.75	0.75	0.75	0.75	0.75	0.75
Draindown at Production Temperature (%)	—	—	—	—	—	—	0.30

^[1] The percent maximum density at initial compaction is only a guideline.

^[2] Represents the percent of the binder of the mixture (as determined by AASHTO T 289) that is retained on the No. 20 sieve.

1. Traffic

2. Aggregates Properties

3. Gyration

4. Densification

Va @ N ini , Va @ Ndes
Va @ N max

5. Durability

Dust/Bind, VFA

TSR

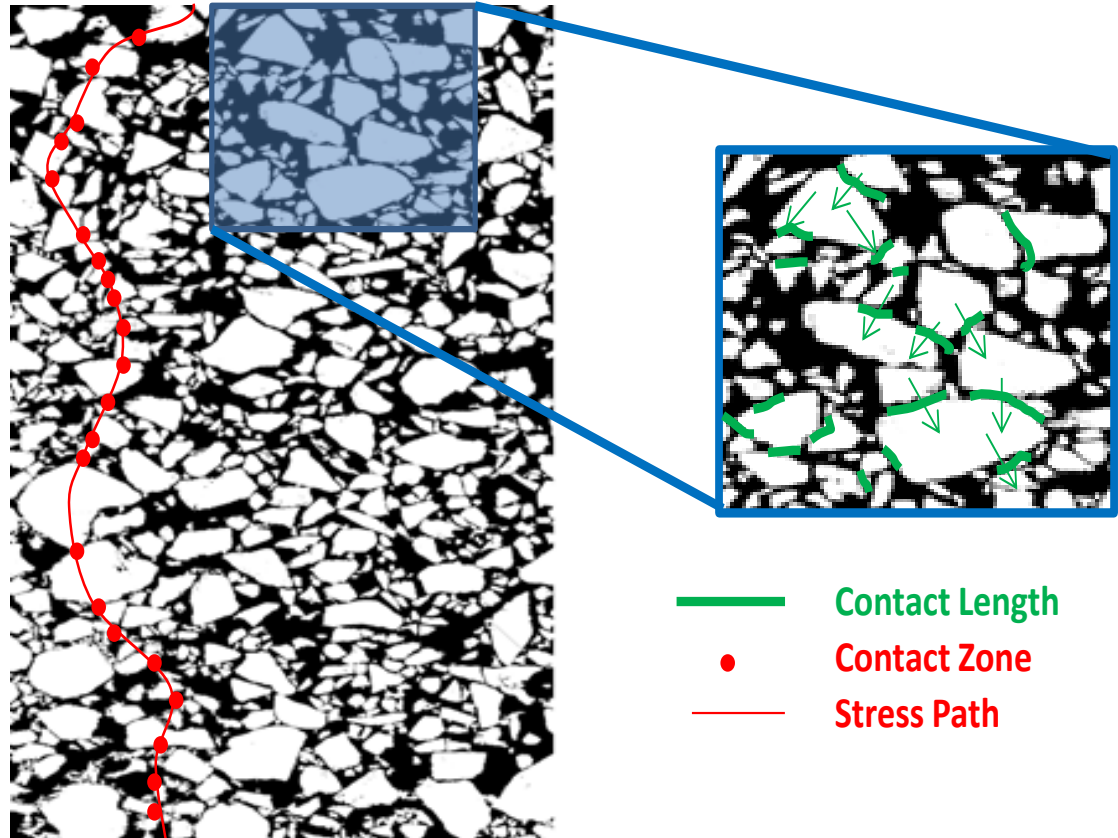
Example of Mixture Specification

Wisconsin DOT

MARC studies: We Measure aggregate structure

iPas1 ... iPas2 ... (Image Processing and Analysis Software)

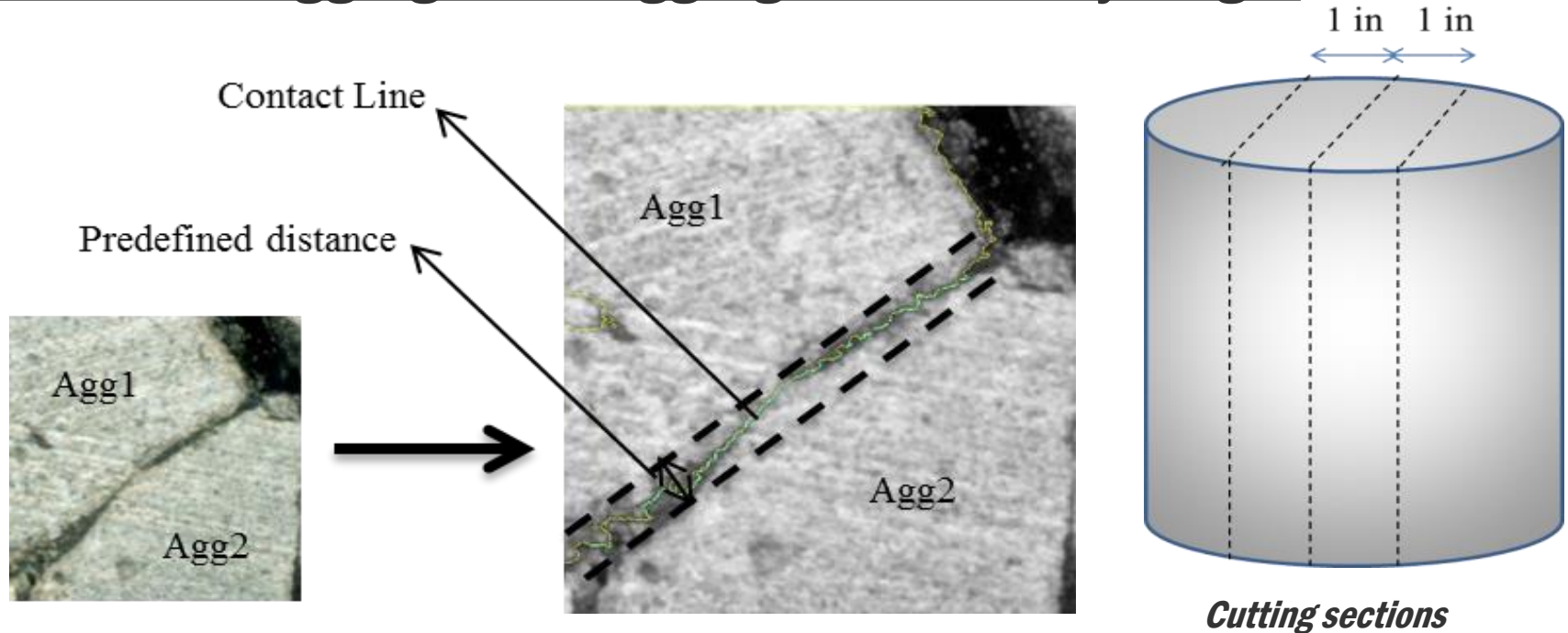
- iPas: A tool to identify aggregate structure.
- Give statistics about
 - Packing
 - Connectivity
 - Orientation
 - Spatial segregation



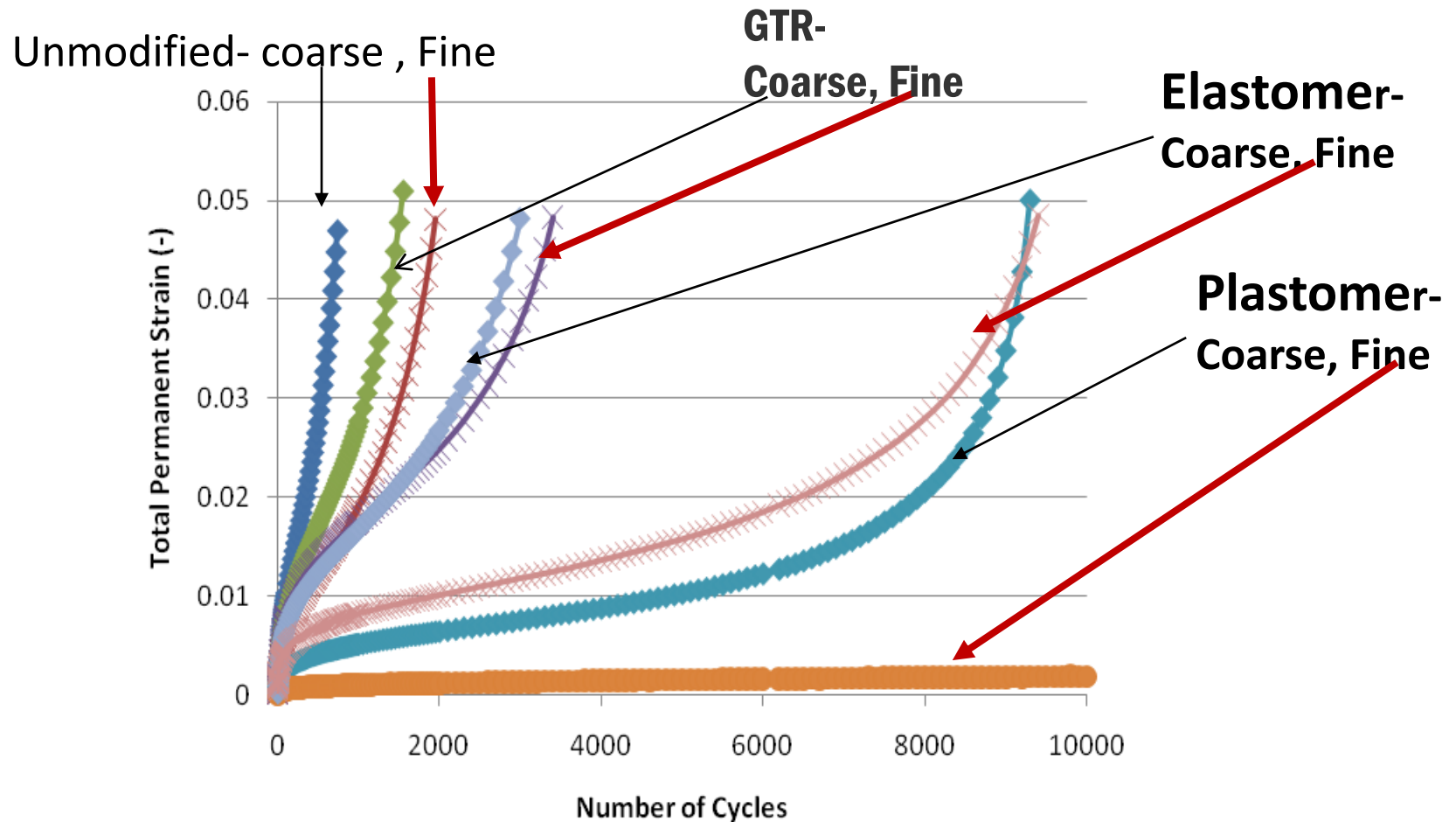
Aggregate Packing Characterization 2D to represent 3D - Stereology

iPas2 output used to quantify packing: Aggr. Proximity Index

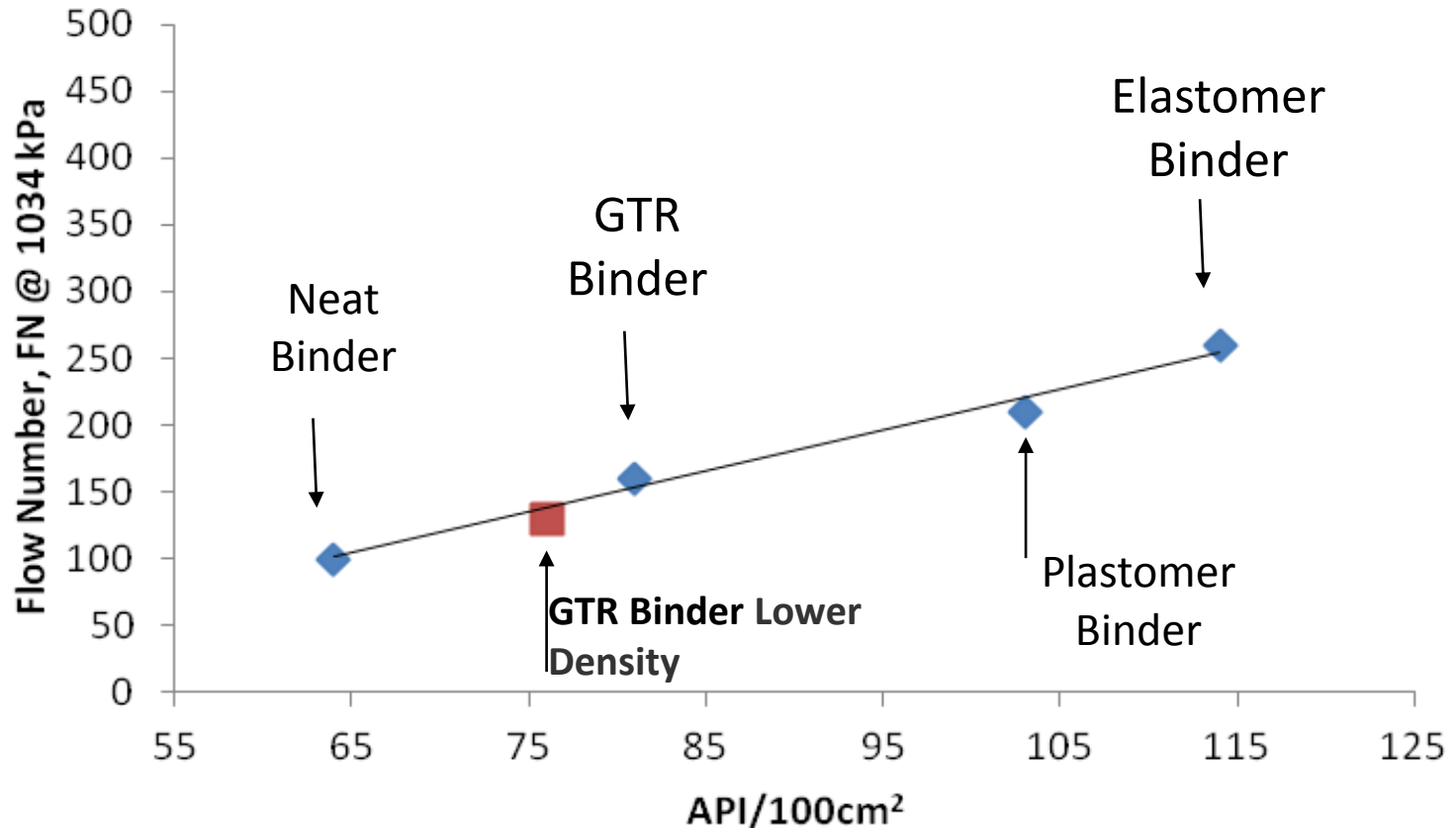
API = Total aggregate to aggregate Proximity length



Can we control Mixture Rutting: Effect of Aggregate Gradation and Binder Modification

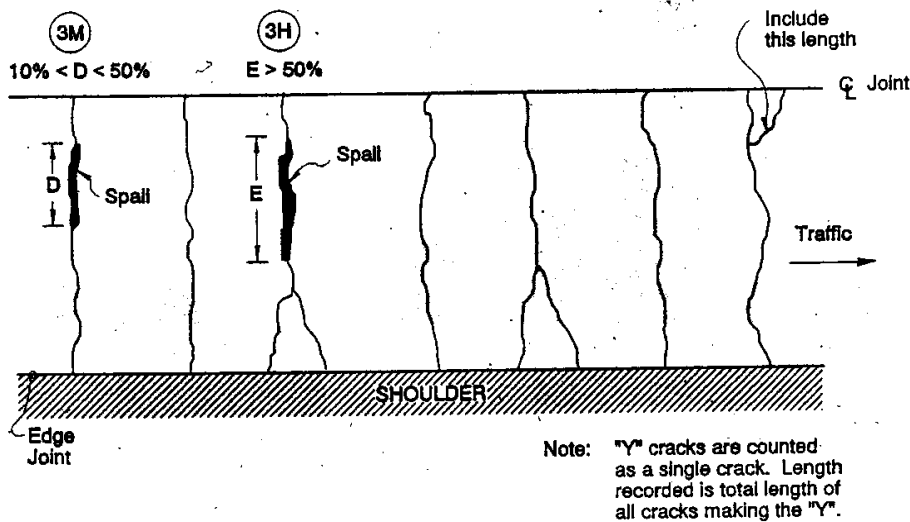


Internal Aggregate Structure (API) Can explain the differences in FN



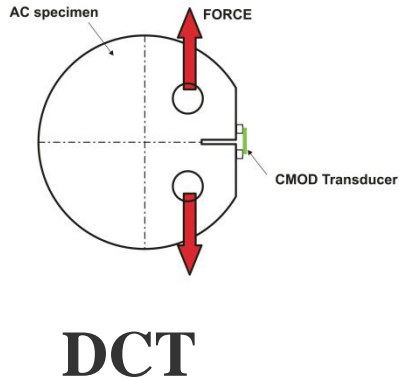
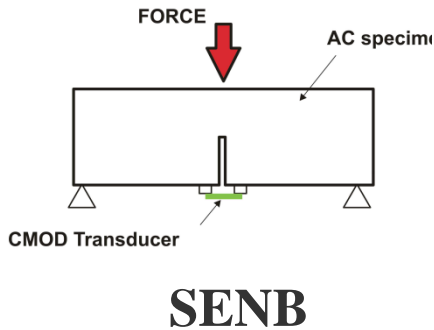
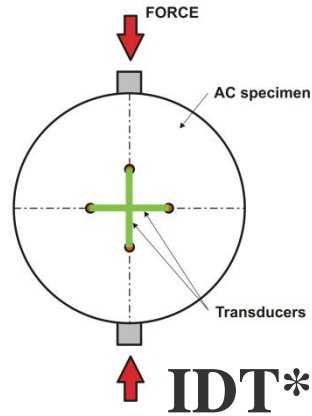
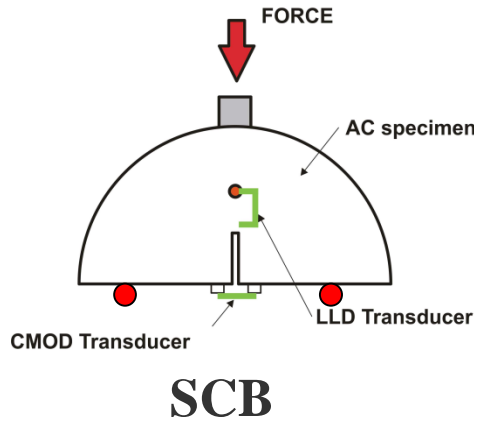
Estonia Cold Climate – Thermal Cracking

- Thermal cracking of pavements **remains one of the most challenging distress** in pavements to predict, and reduce, in North America.



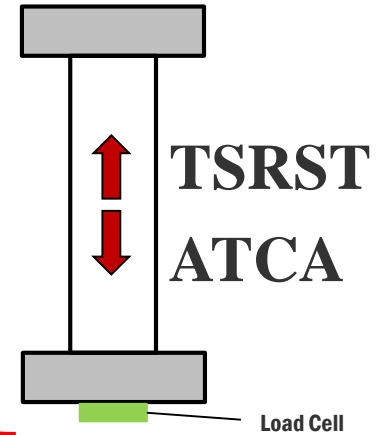
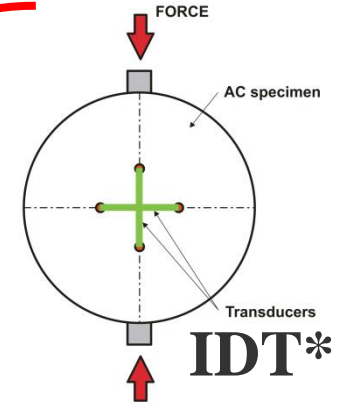
Cold Temperature Mixture Test Methods:

Two types



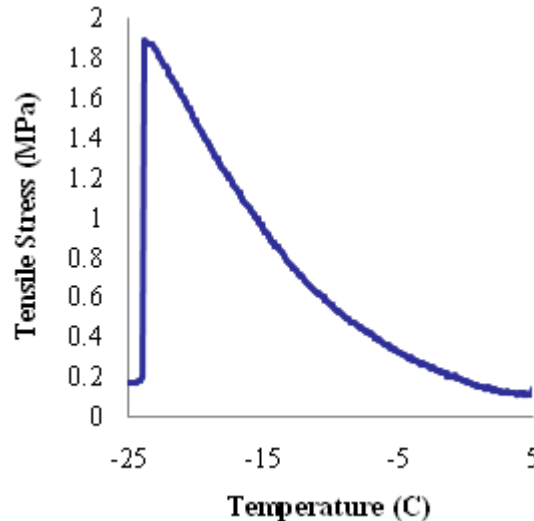
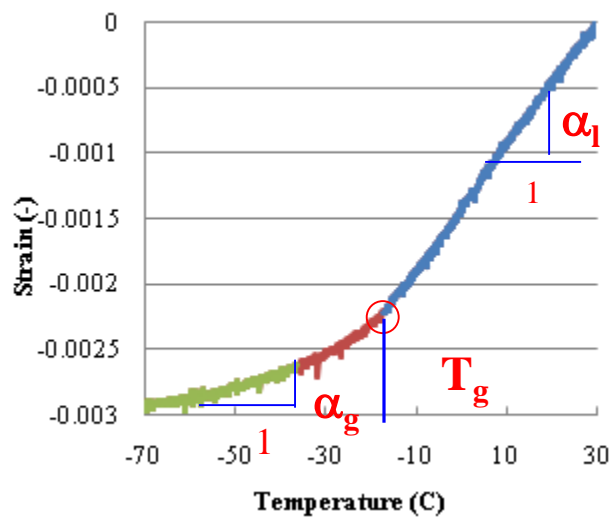
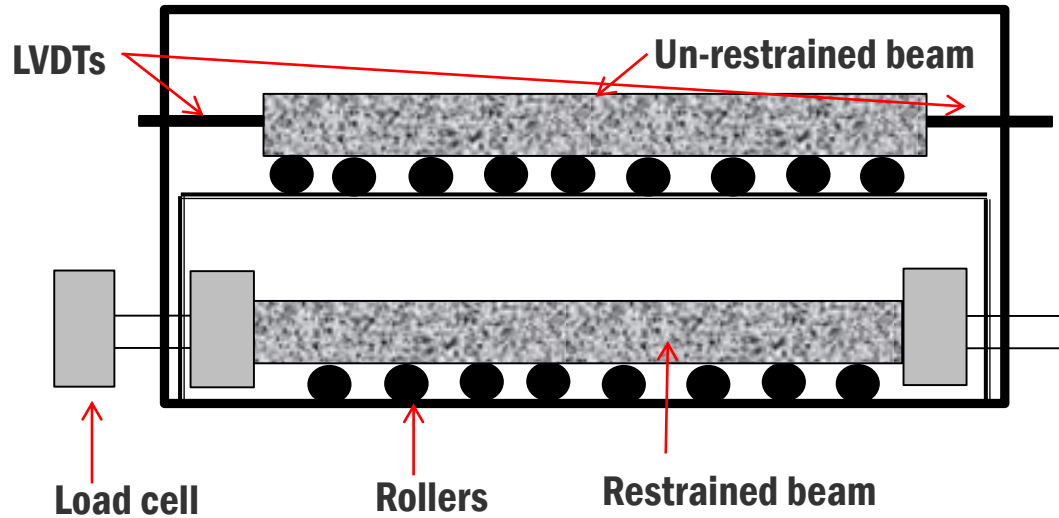
1. Fracture Tests

2. Modulus & Failure Tests

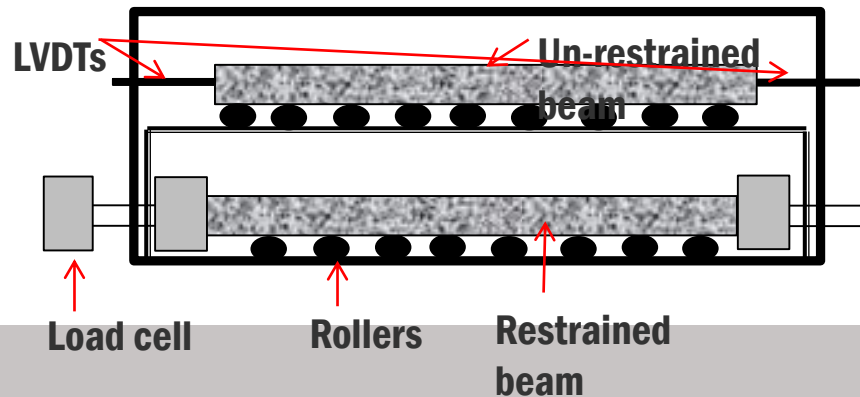
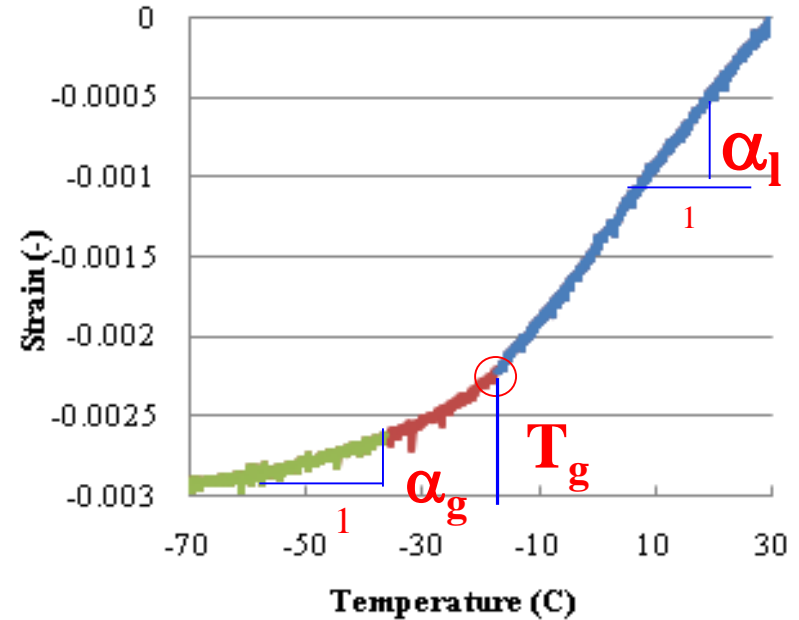
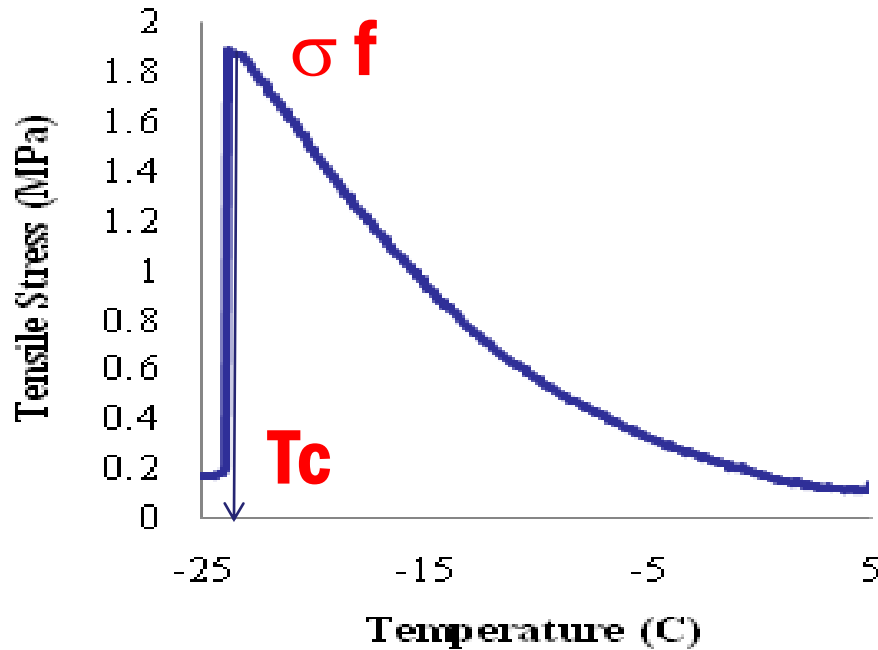


*IDT can be performed with notch (fracture), without notch (failure) or in creep mode.

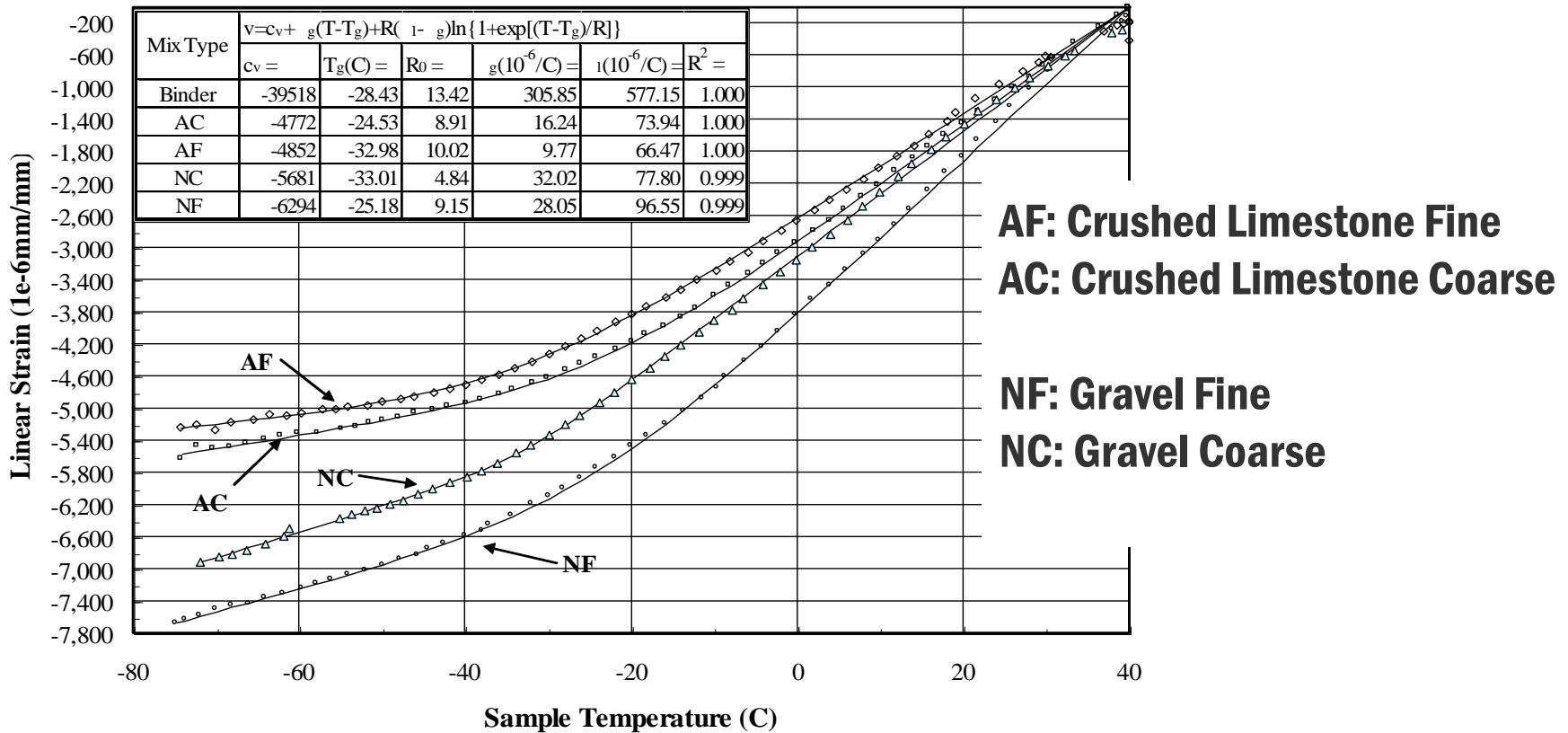
ATCA: Asphalt Thermal Cracking Analyzer



ATCA: Asphalt Thermal Cracking Analyzer

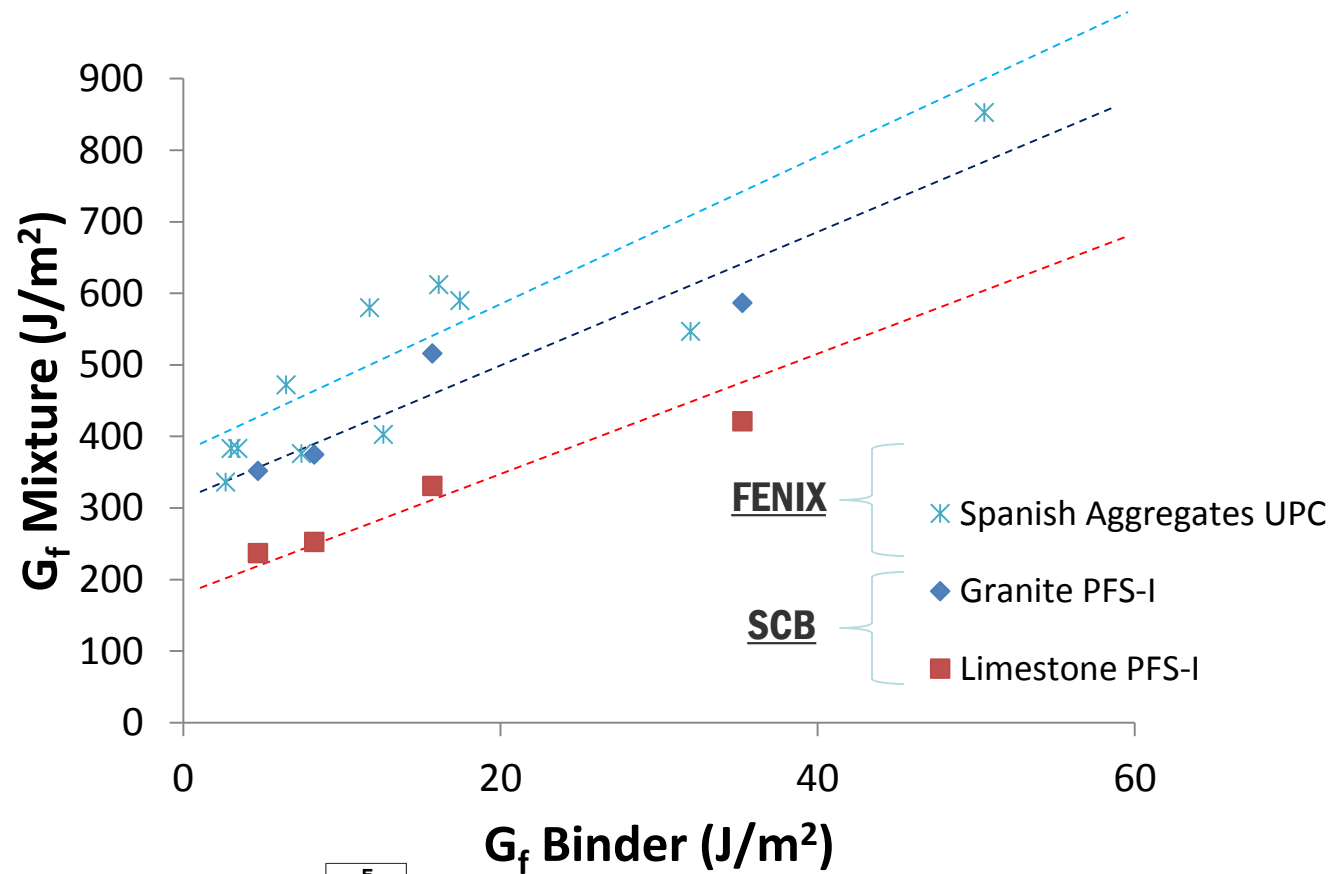


Aggregate Type Effect on Contraction Coefficients and Tg

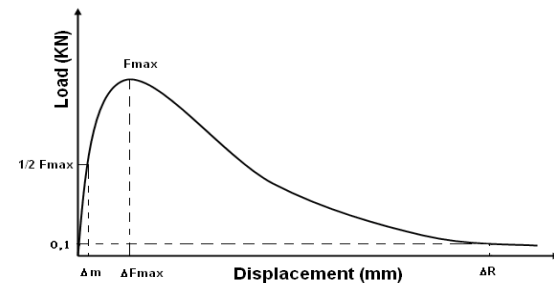
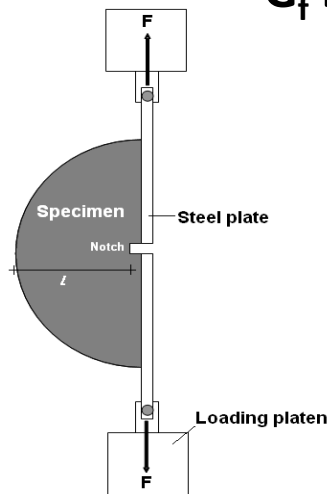


same binder and similar binder content

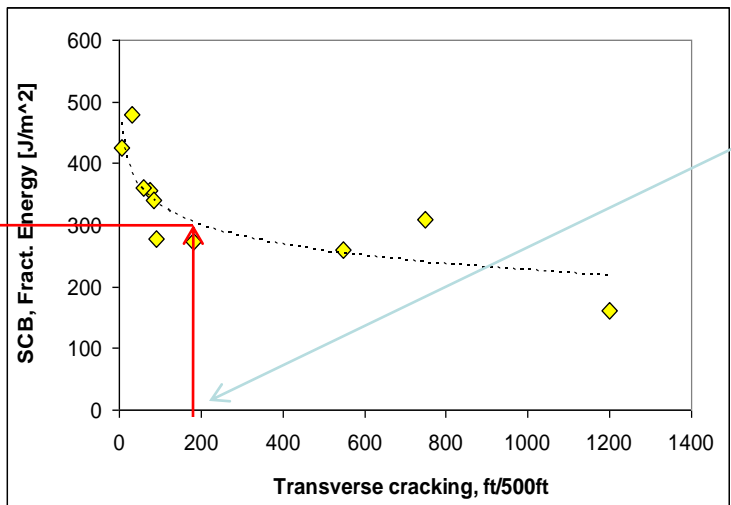
Binders vs. Mixtures



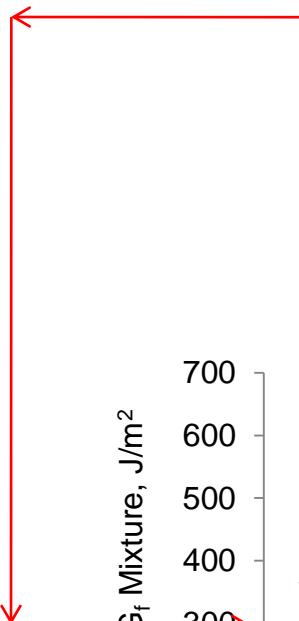
Fenix Test (Mixtures)



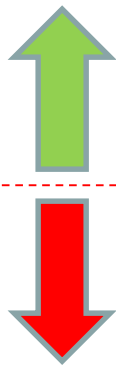
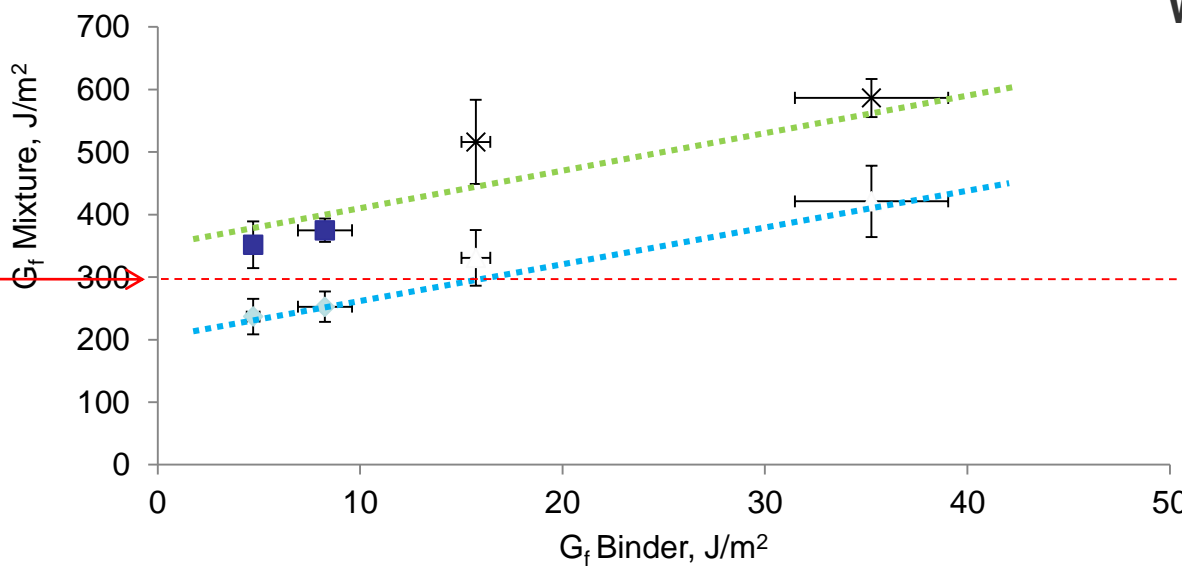
Developing Material Selection Criteria



If **200 ft/500 ft** of transverse cracking after 5 years is acceptable



Acceptable Mixtures: All granite and limestone with binder $G_f > 15 \text{ MJ/m}^2$



Unacceptable Mixtures: limestone with binder $G_f < 15 \text{ MJ/m}^2$

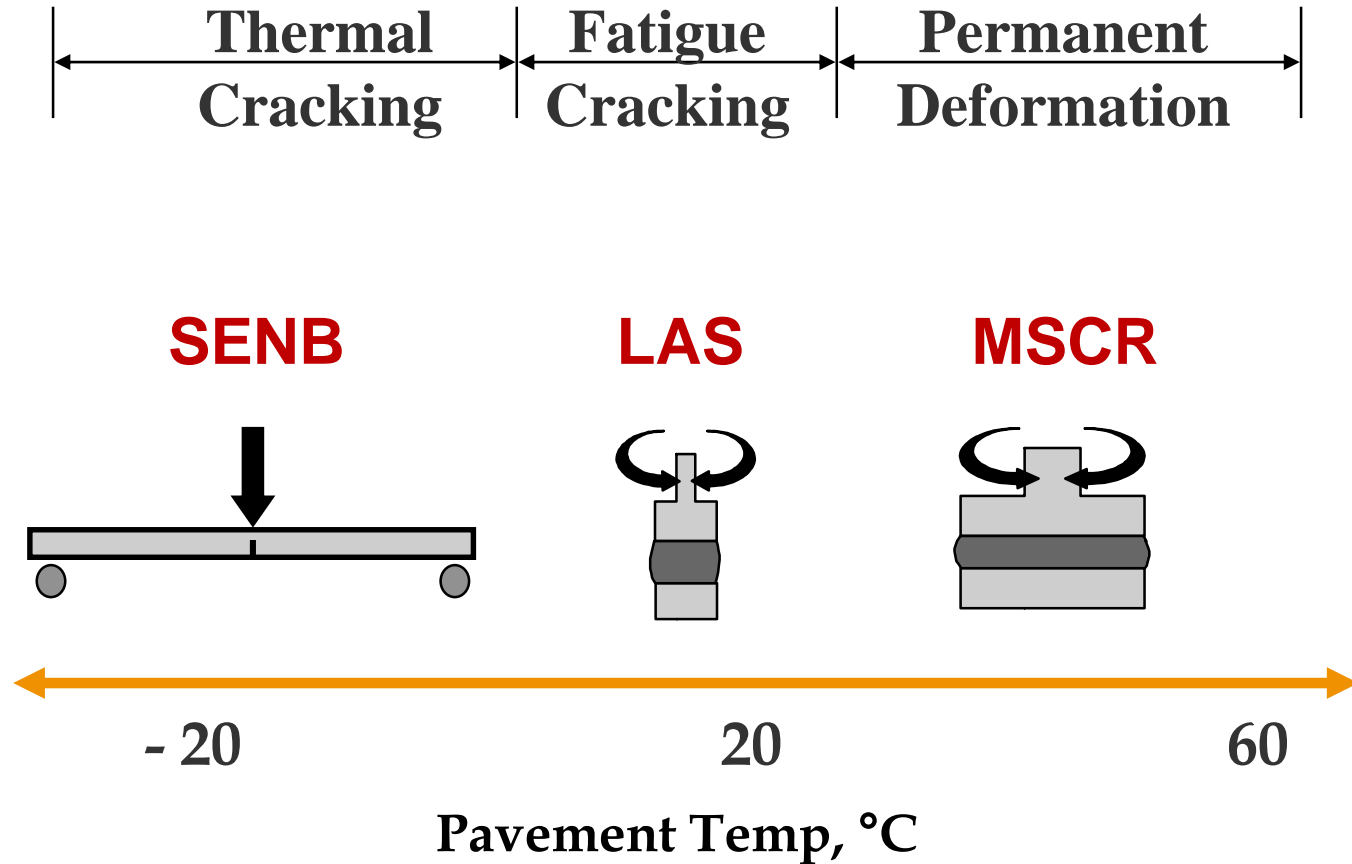
- ◆ Limestone Low Temp
- △ Limestone Int Temp
- Granite Low Temp
- × Granite Int Temp

Estonia Study – Hypothesis & Objectives

- **Hypothesis:**
 - Variety of available bitumen types in Estonia does not adequately cover the varying climatic needs.
- **Objectives:**
 - Conduct Superpave performance grading testing protocol to determine the PG grades of Estonian binders.
 - Compare the grades of available binders with those required for existing climatic conditions.
 - Investigate the production of needed grades through feasible modification techniques.

New Methods for Modified Binder Evaluation

Damage – Based Characterization



Required PG Grades

PG 58-28

PG 58-34

PG 58-40



Materials

Binders' designations provided from different crude sources

Binder Code	Description	Crude Oil	PG
A	Pen 70-100	Venezuela	64-22
B	Pen 70-100	Russia	58-22
C	Pen 70-100	Russia	58-22
D	Pen 70-100	Russia	58-28
E	Pen 70-100	Russia	70-28
F	Pen 160-220	Venezuela	52-28
G	Pen 160-220	Russia	52-28
H	Shale Oil	Estonia	52-4

Available vs. Required PG Grades

●	Available PG
○	Needed, Unavailable PG

		High Service Temperature			
		52	58	64	70
Low Service temperature	-22	●	●	●	
	-28		●		●
	-34		○		
	-40		○		

Modification Alternatives: Oils + Polymers

Base Binder	Modification	Modified Binder Code	PG
A	5% Oil-A	M-A	58-28
B	10% Oil-B + 2% Plastomer	M-B	58-34
C	8% Oil-B + 3% Elastomer	M-C	58-34
D	8% Oil-B + 2% Plastomer	M-D	58-34
E	11% Oil-A	M-E-1	58-34
E	8% Oil-B	M-E-2	58-40
F	8% Oil-B + 4% Plastomer	M-F	58-34
G	8% Oil-B + 5% Elastomer	M-G	58-34

- **Oil A: Bio Oil**
- **Oil B: Refined Waste Oil**
- **Elastomer: SBSx**
- **Plastomer: Functionalized Polyethylene (Titan 7686)**

Selection of the **dosage of oil modifier** based on the **required low temperature** performance grade

Test Methods

Test Methods Selected for Binder Evaluation

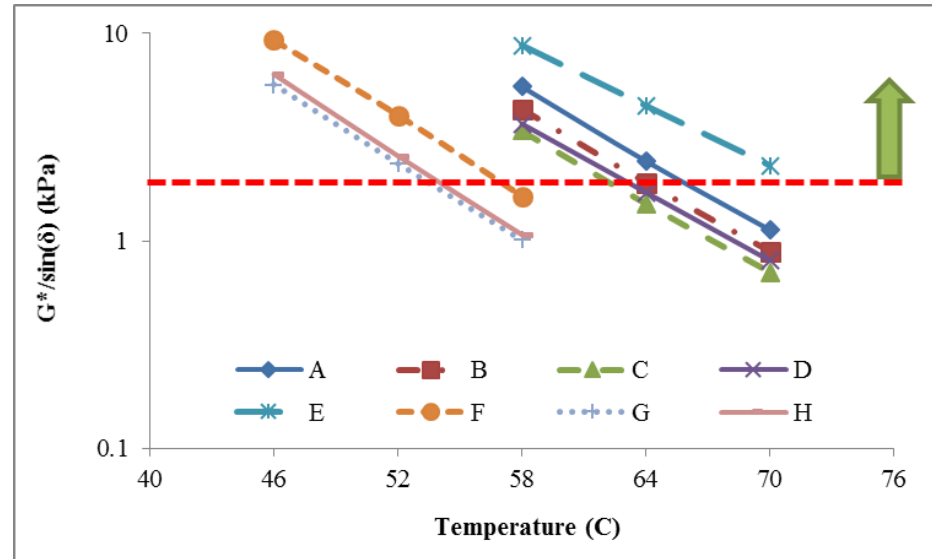
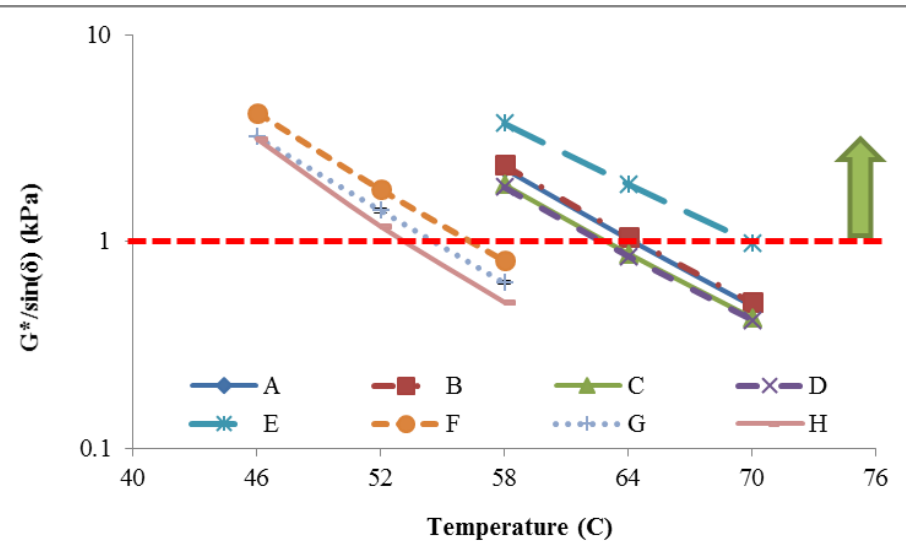
	Engineering Property of the Binder	Conventional Binder Test	Advanced Binder Test
1	Rutting resistance	DSR HT PG	---
2	Fatigue Cracking Resistance	DSR IT PG	Linear Amplitude Sweep (LAS)
3	Thermal Cracking Resistance	Bending Beam Rheometer (BBR)	Single Edge Notched Beam (SENB)
4	Chemical Content Spectrum	---	Gel Permeation Chromatography (GPC)

Results

High Temperature Grading- Unmodified Binders

Un-Aged

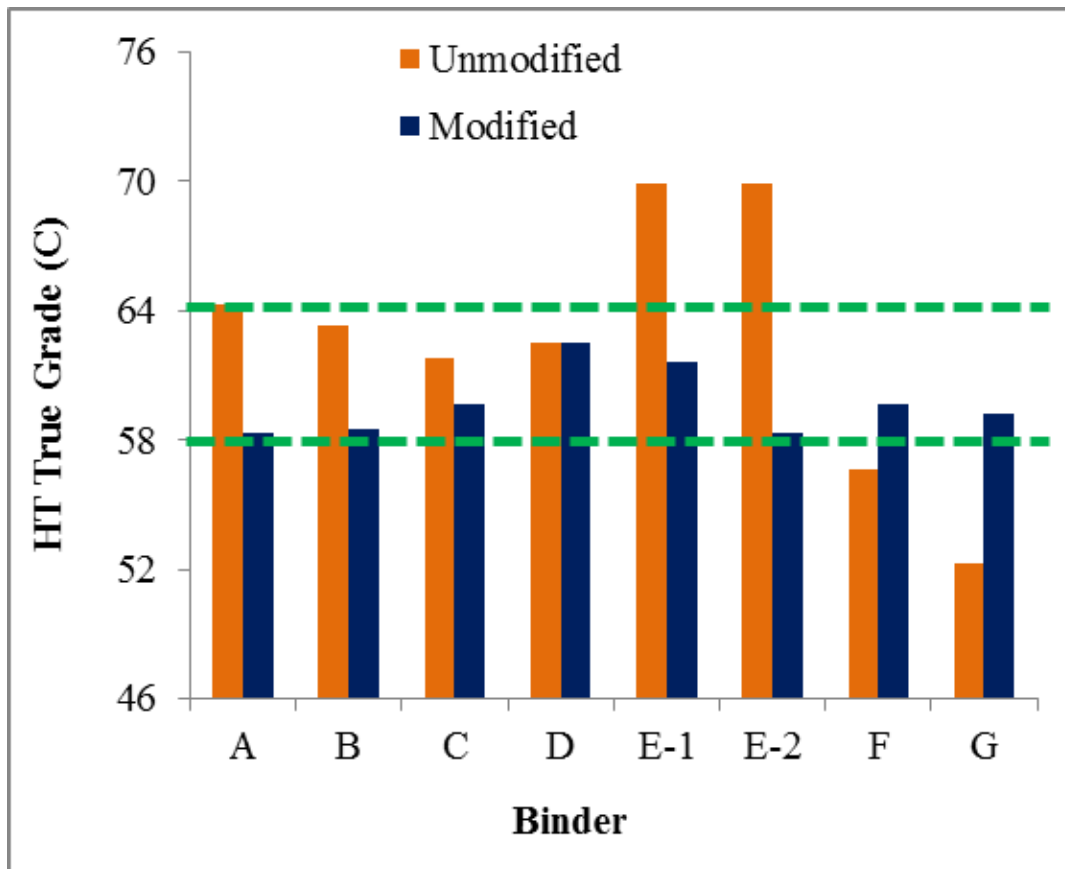
RTFO Aged



Narrow range of Performance Grades between provided Binders

Results

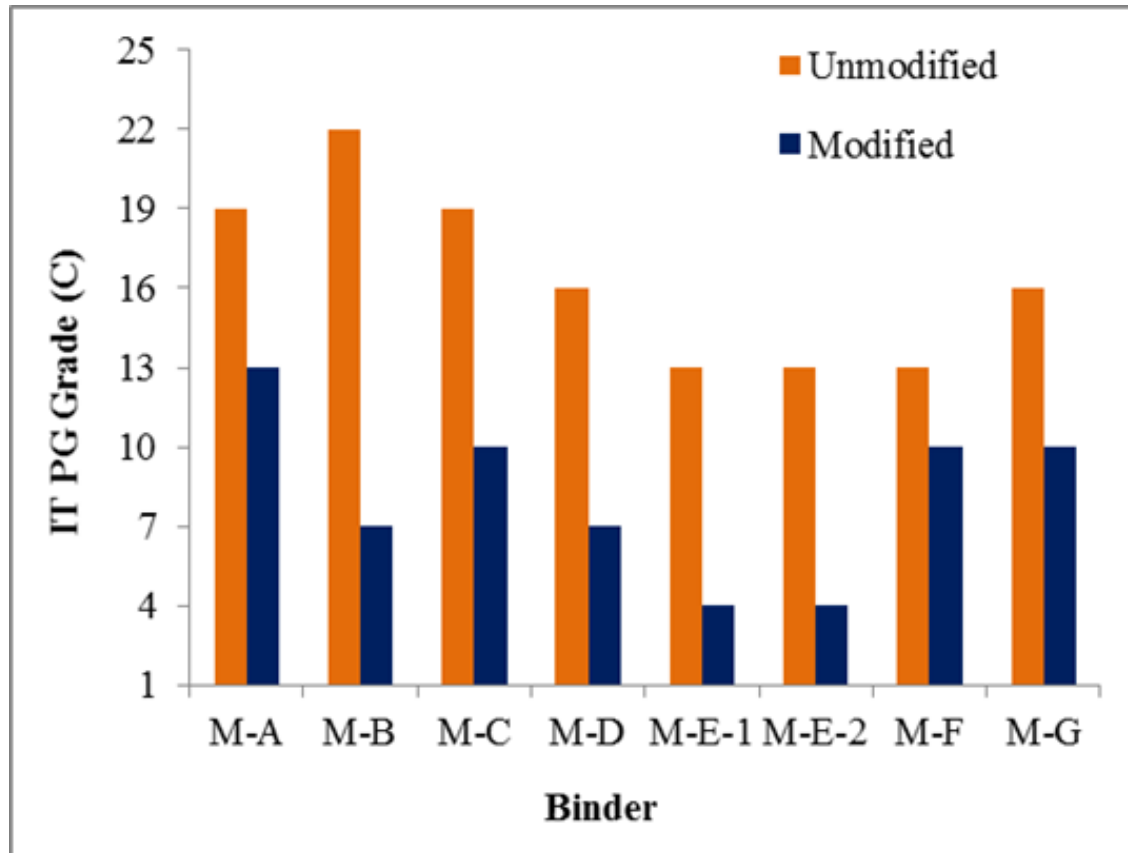
High Temperature Grading- *Continuous Grade*



- binders **with same pen grade (i.e binder A to E)** showed different behavior at high temperatures and **cover a range of three different PG grades**
- adding lubricating oils decrease the high temperature properties of the original binder

Results

Intermediate Temperature Continuous Grade

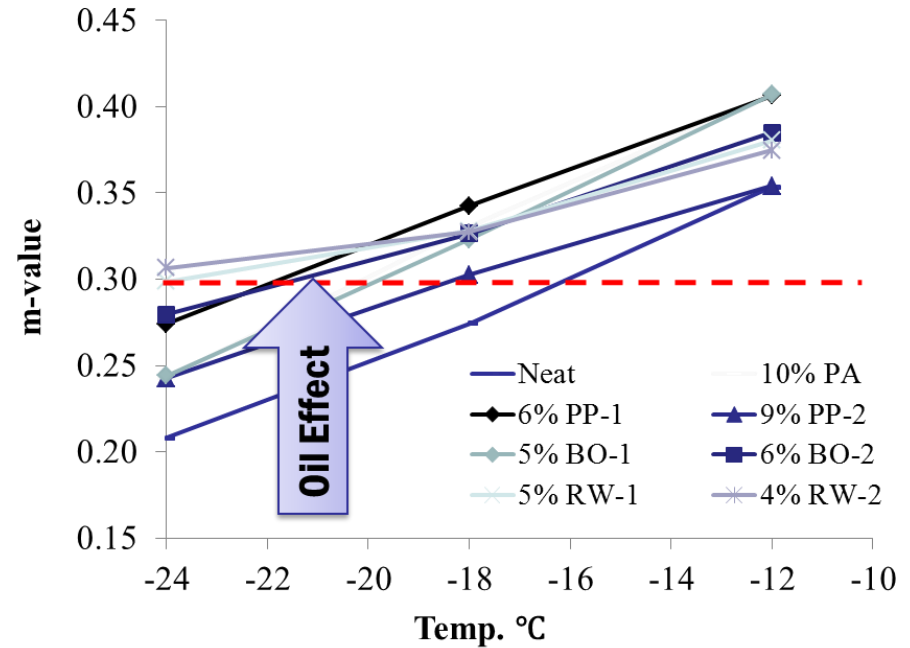
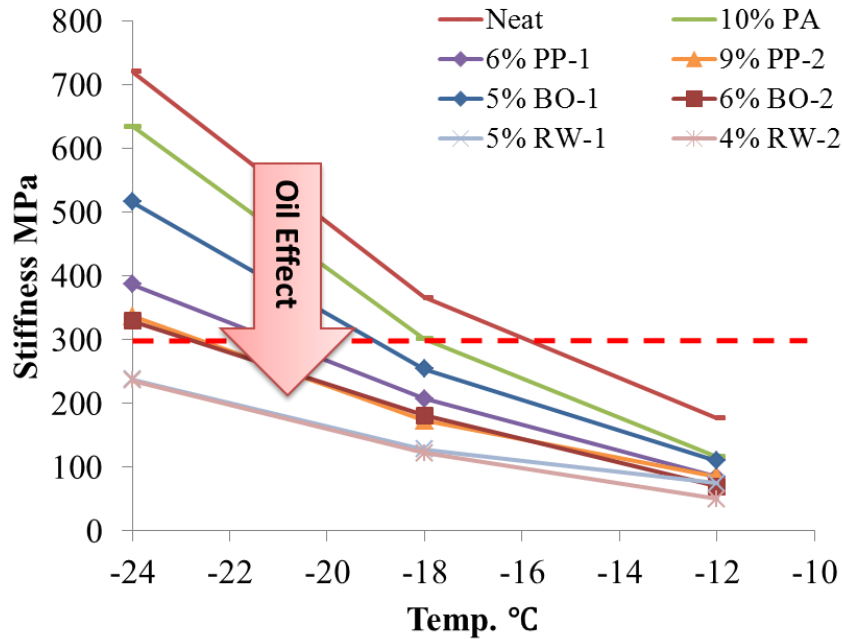


Reduction in the IT grade of binders by 6 to 15°C by binder modification

Superpave Max IT Grade:

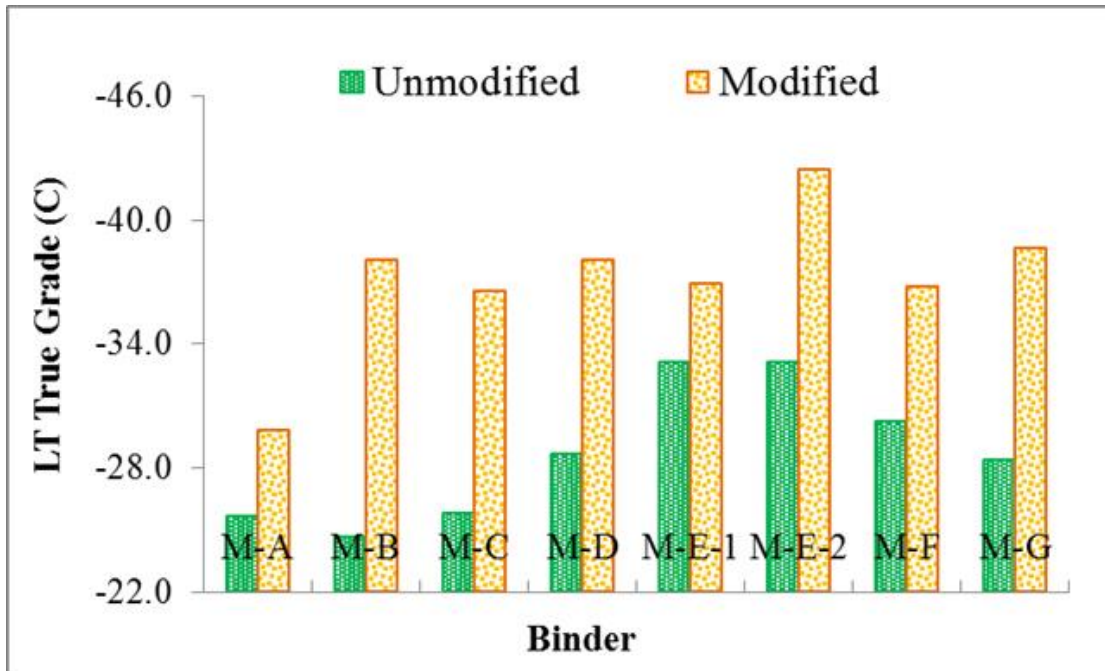
- **PG 58-28: 19°C**
- **PG 58-34: 16°C**
- **PG 58-40: 13°C**

Effect of Oils on LT Binder Properties



Results

Low Temperature Grading- *Continuous Grade*



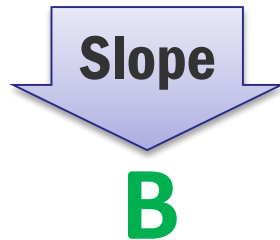
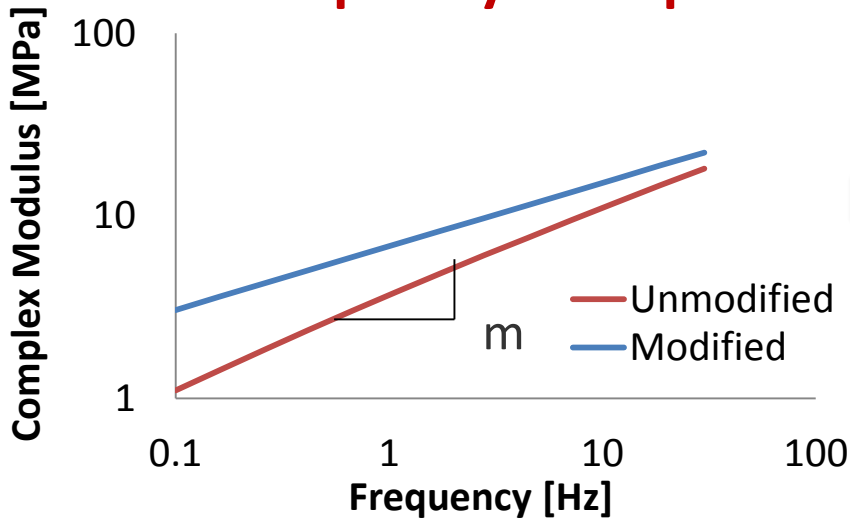
➤ Considering the high temperature grade of these binders to be kept the same level, **selected modifications** were capable of expanding the performance range of binders by **shifting the lower band up to 10°C**

Fatigue Life from LAS

Specification based on Binder Nf

Rheology

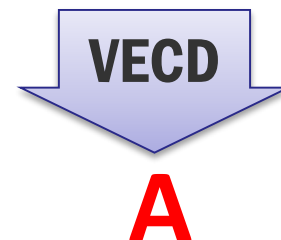
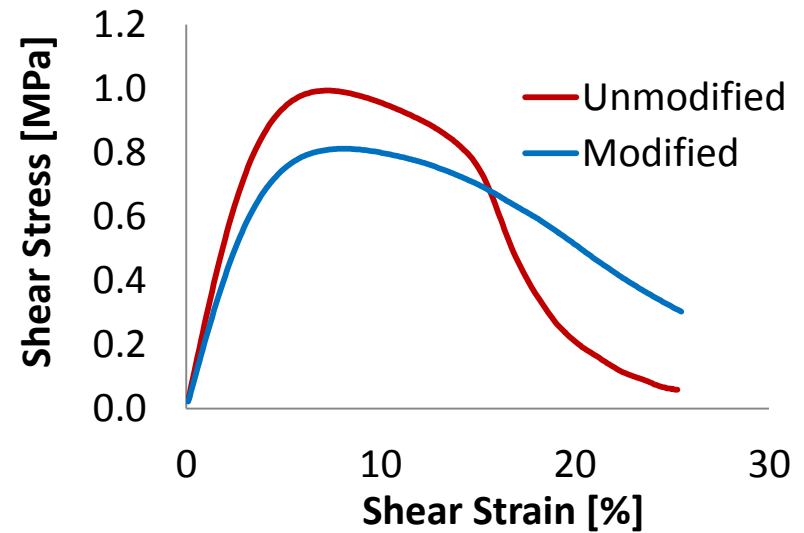
Frequency Sweep



$$N_f = A (\gamma_{max})^B$$

Damage Resistance

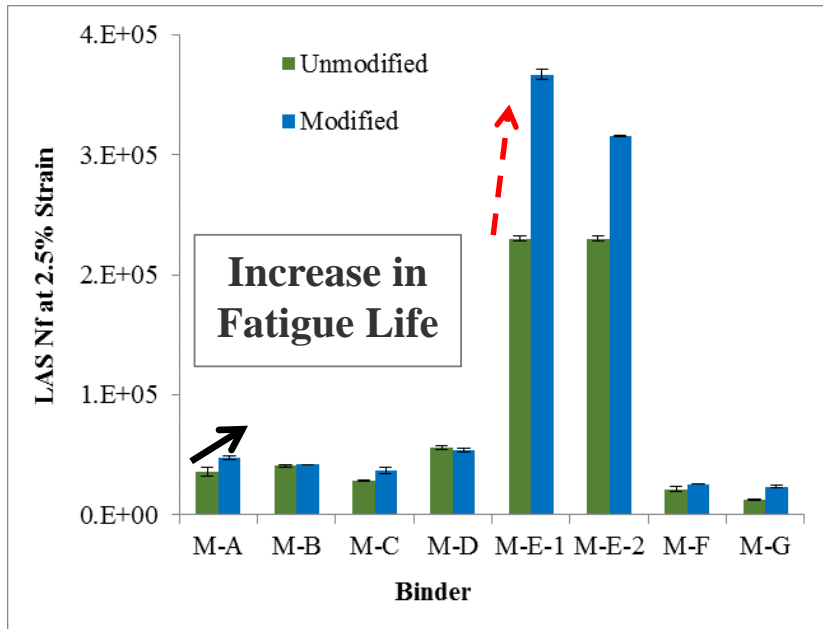
Continuous Amplitude Sweep



Results

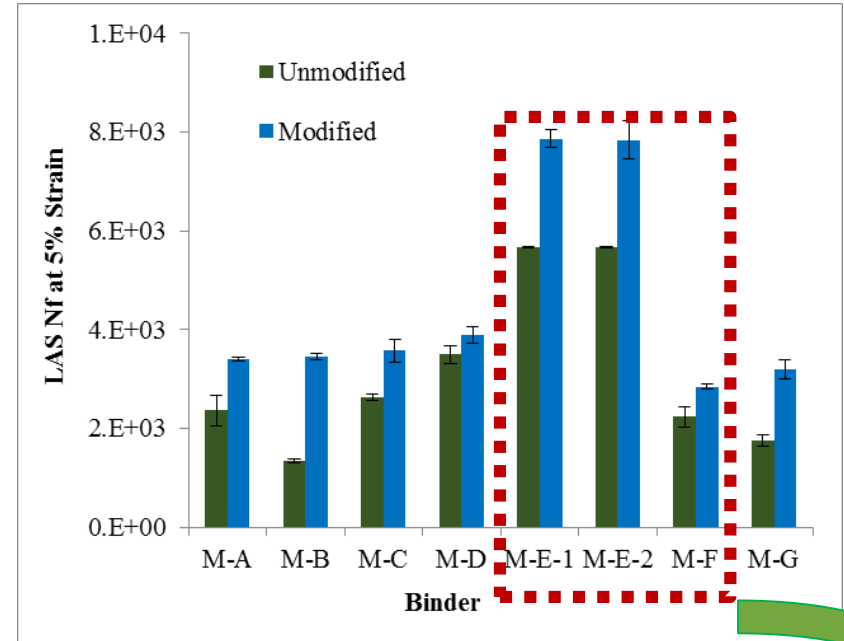
Linear Amplitude Sweep (LAS) Test

2.5% Strain Amplitude



Lubricating oils improve the fatigue resistance at different strain levels

5% Strain Amplitude



Same IT PG grade can resist fatigue significantly different

Single Edge Notched Bending (SENB)

Displacement-Controlled Mode



Step Motor



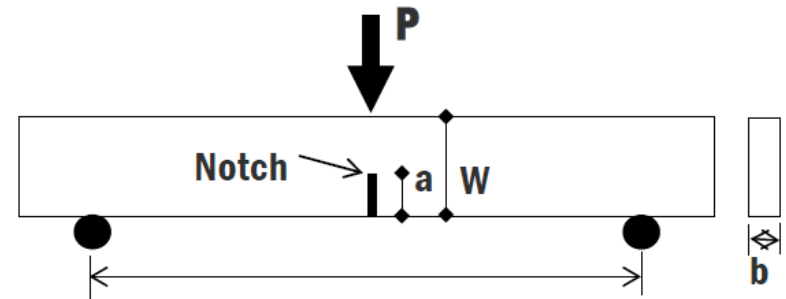
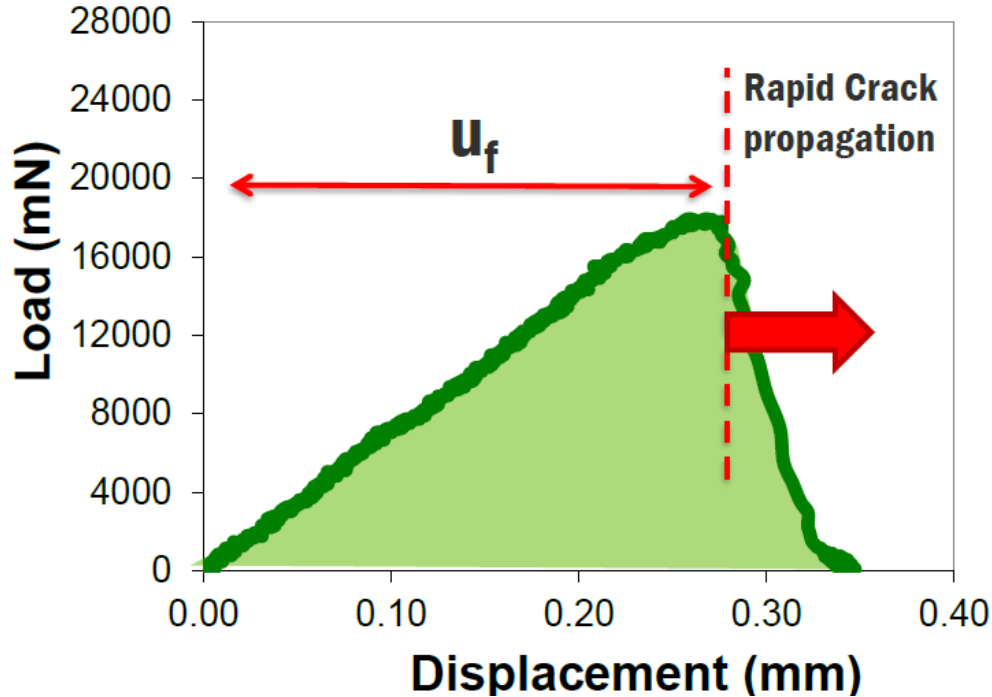
BBR system
with a load cell
with **higher**
capacity



Fracture Properties and Strain Tolerance

Single-Edge Notched Beam (BBR-SENB):

- Failure Energy (G_f)
- Deflection at failure (u_f)

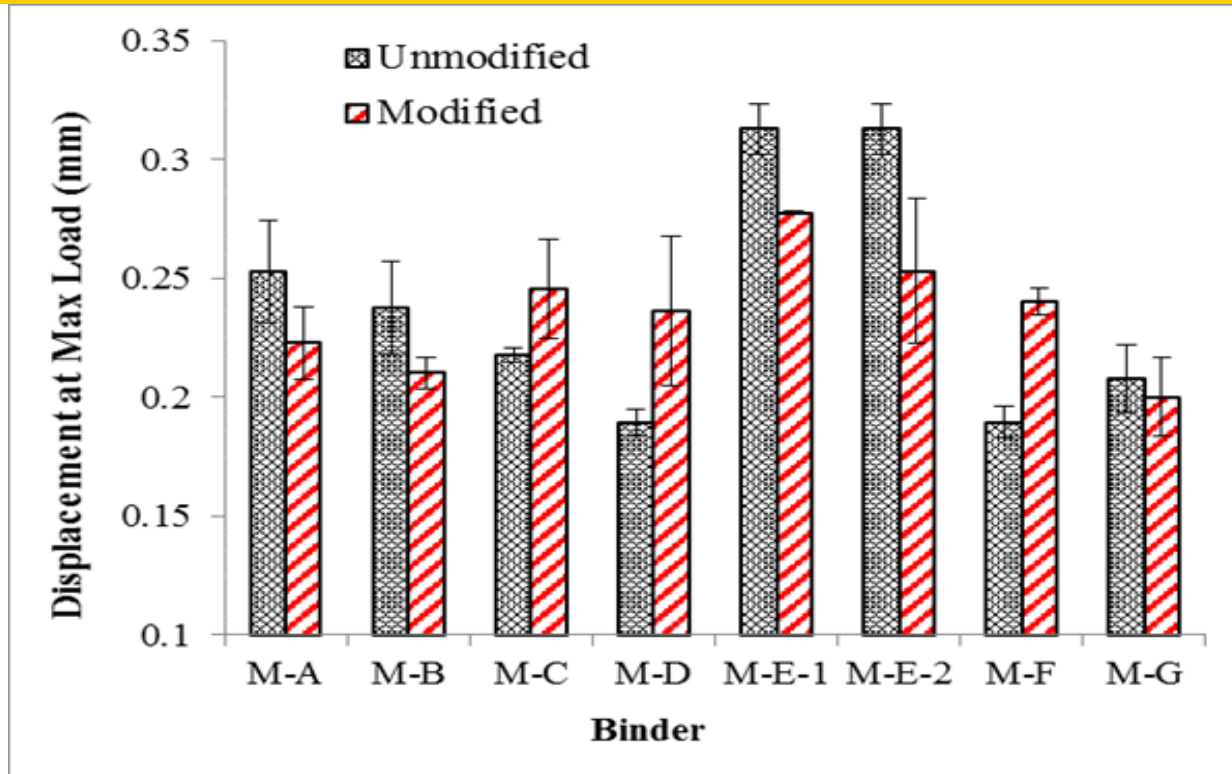


$$G_f = \frac{W_f}{A_{lig}} \quad \text{Failure Energy}$$

$$W_f = \int P du \quad \text{Work}$$

Results

Single Edge Notched Bending (SENB) @ LT Grade



- Marginal difference between unmodified and modified binders
- Test is performed at LT grade of the binders

Concluding Remarks- Binder Study

- **Estonia will need to use Oil modification to improve performance of pavements**
- **Oils could result in lower rutting resistance; need polymers to offset this effect**
- **Fatigue resistance varies significantly based on oils**
- **Impact of oils and polymers vary based on oil type and the crude source of binder**

Concluding Results – General

- **Roads are built with mixtures, not Binders!**
- **Thermal Cracking & rutting are affected by:**
 - aggregate structure and binder properties.
- **Suggestion for Mixture studies:**
 - Internal structure and resistance to rutting
 - Ipas and FN
 - Coefficient of thermal contraction- ACTA
 - Fracture properties
 - Moisture damage – Wet Hamburg

Thank You!

Questions?

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MARC MODIFIED ASPHALT RESEARCH CENTER
Part of the Asphalt Research Consortium

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BBR-SENB
The BBR-SENB system is a modification of the Bending Beam Rheometer, that enables low temperature fracture testing on BBR size beams.
MARC continues to evaluate the potential of the BBR-SENB system for better estimation of the thermal cracking susceptibility of asphalt materials.

Image from Marasteanu (2007)

LATEST NEWS

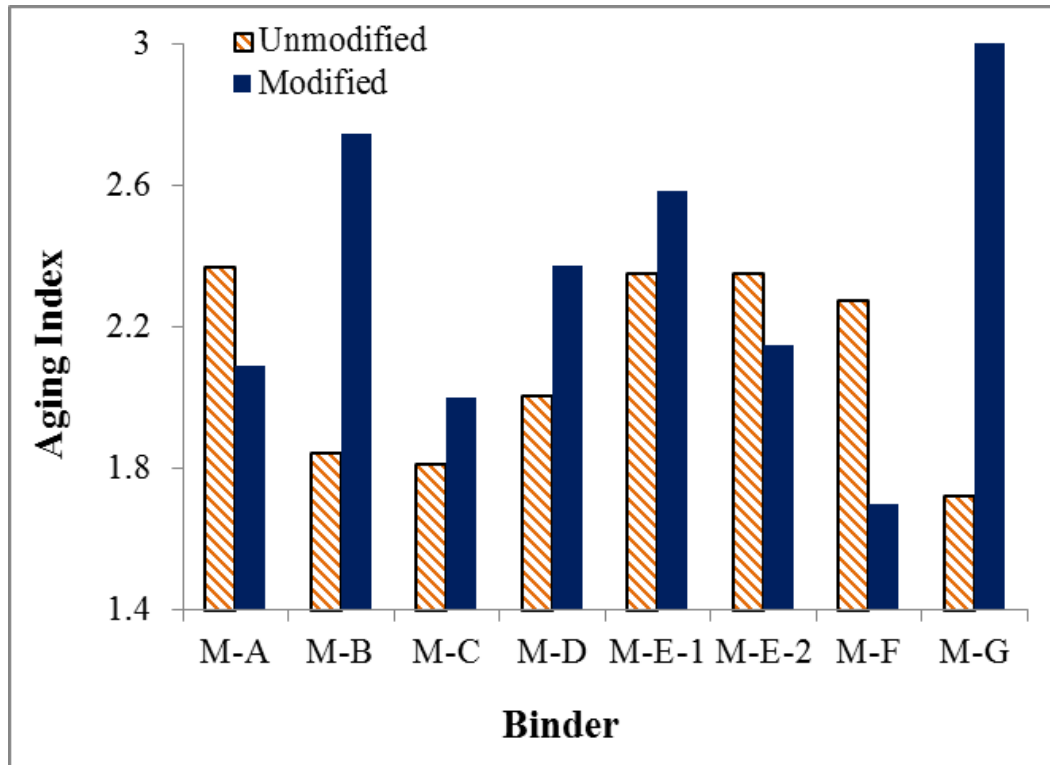
MARC JOINS NCHRP PROJECT 9-50
Jan 30, 2011 – The Modified Asphalt Research Center at UW Madison has joined North Carolina State University's research team to submit a proposal for the new NCHRP 9-50 project, "Performance-Related Specifications for Asphaltic Binders Used in Preservation Surface Treatments." This project will focus on the development of performance-related specifications (PRS) for asphaltic binders used in preservation surface treatments, usually applied to large pavement surface areas to slow rate of deterioration and maintain or improve its functional condition. The project is expected to start early summer of 2011. More information can be found at the [NCHRP Project webpage](#)?

LATEST EVENTS

MARC TRAINS ETG MEMBERS IN USE OF THE LINEAR AMPLITUDE SWEEP TEST
Feb 22, 2011 – MARC held a webinar on Feb 22 in which Ms. Cassie Hintz and Dr. Raul Velasquez explained the conduction and analysis of the newly introduced Linear Amplitude Sweep (LAS) binder fatigue test. Participants were shown videos of the LAS procedure implementation into commonly used Dynamic Shear Rheometers (DSR). The session also included a demonstrated of the use of the LAS analysis spreadsheet and data interpretation. The meeting was ended with a question and answer session held by Dr. Velasquez on the test theory and procedure.

Results

High Temperature Grading-Aging Susceptibility

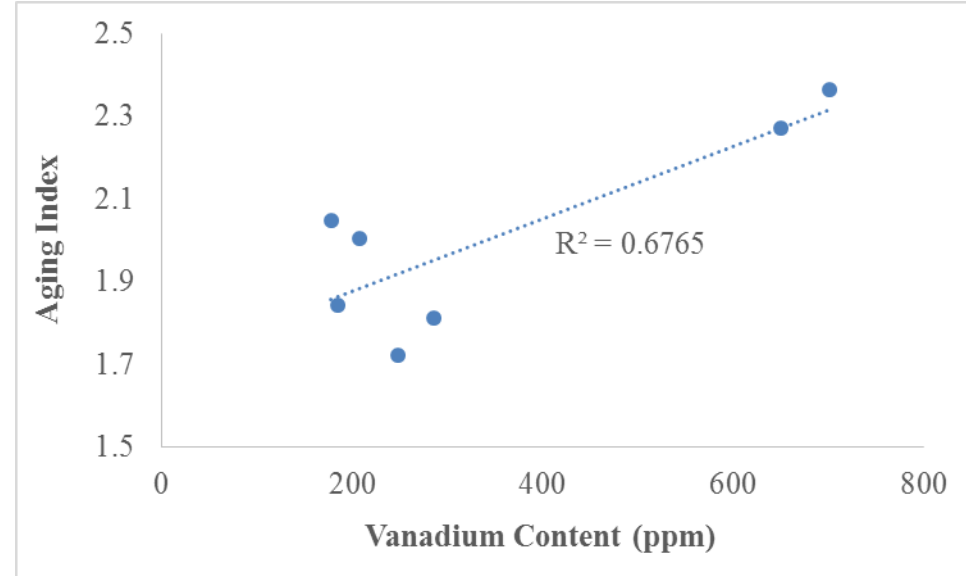
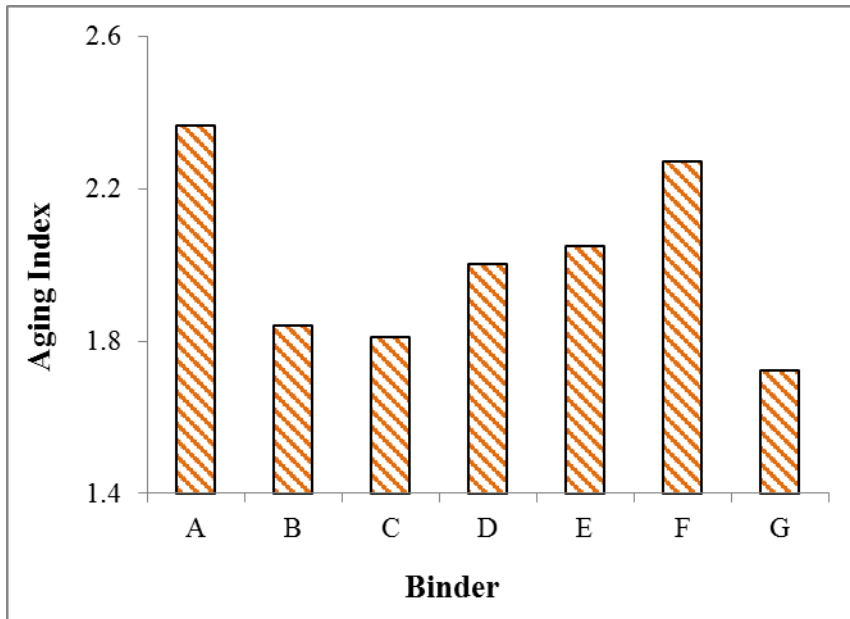


$$A. I. = \frac{\frac{G^*}{\sin\delta} RTFO}{\frac{G^*}{\sin\delta} OB}$$

- **Aging effect** of different recycling agents are **not the same**
- The difference in aging index for different recycling agents comes from their **different chemical components**
- Values will change if the binder is exposed to long term aging

Results

Aging Vs. Elemental Analysis



$$\text{Aging Index} = \frac{\text{RTFO Aged } |G^*| / \sin \delta}{\text{Un-aged } |G^*| / \sin \delta}$$

Aging Susceptibility has fair relationship to Vanadium Content

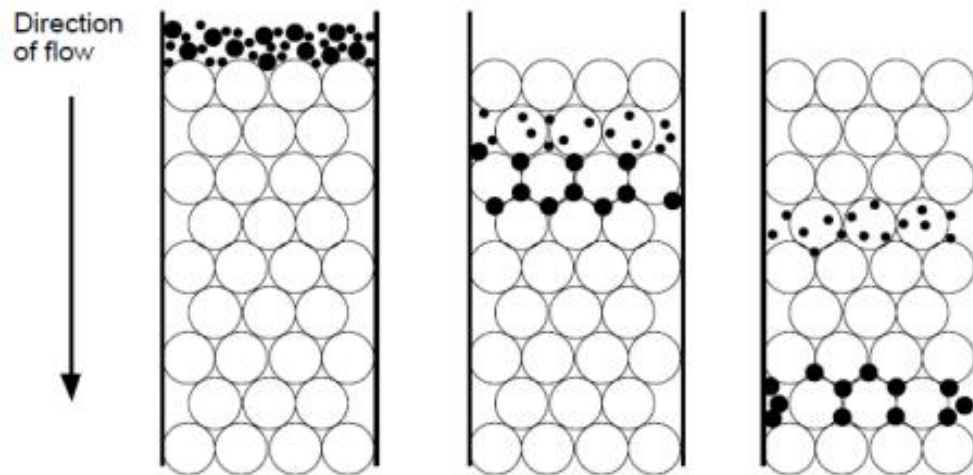
GPC Parameters

- **MW: weight-average molecular weight**
 - influences the bulk properties and toughness of the material
- **Mn: number-average molecular weight**
 - influences the thermodynamic properties of the molecule
- **Mz: z-average molecular weight**
- **Mp: peak molecular weight**

Gel Permeation Chromatograph (GPC)

- Simple separation technique available that **responds to molecular size alone** and not to chemical structure.

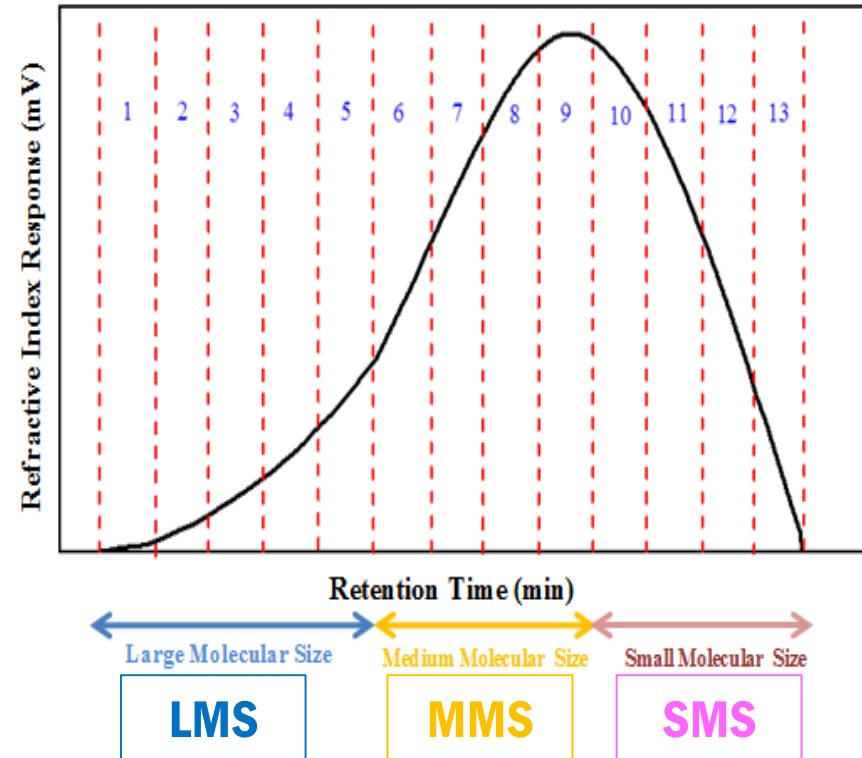
- Analogous to a type of sieve analysis of sample.



● Molecules larger than the largest pores of the swollen gel particles

● Molecules small enough to penetrate gel particles

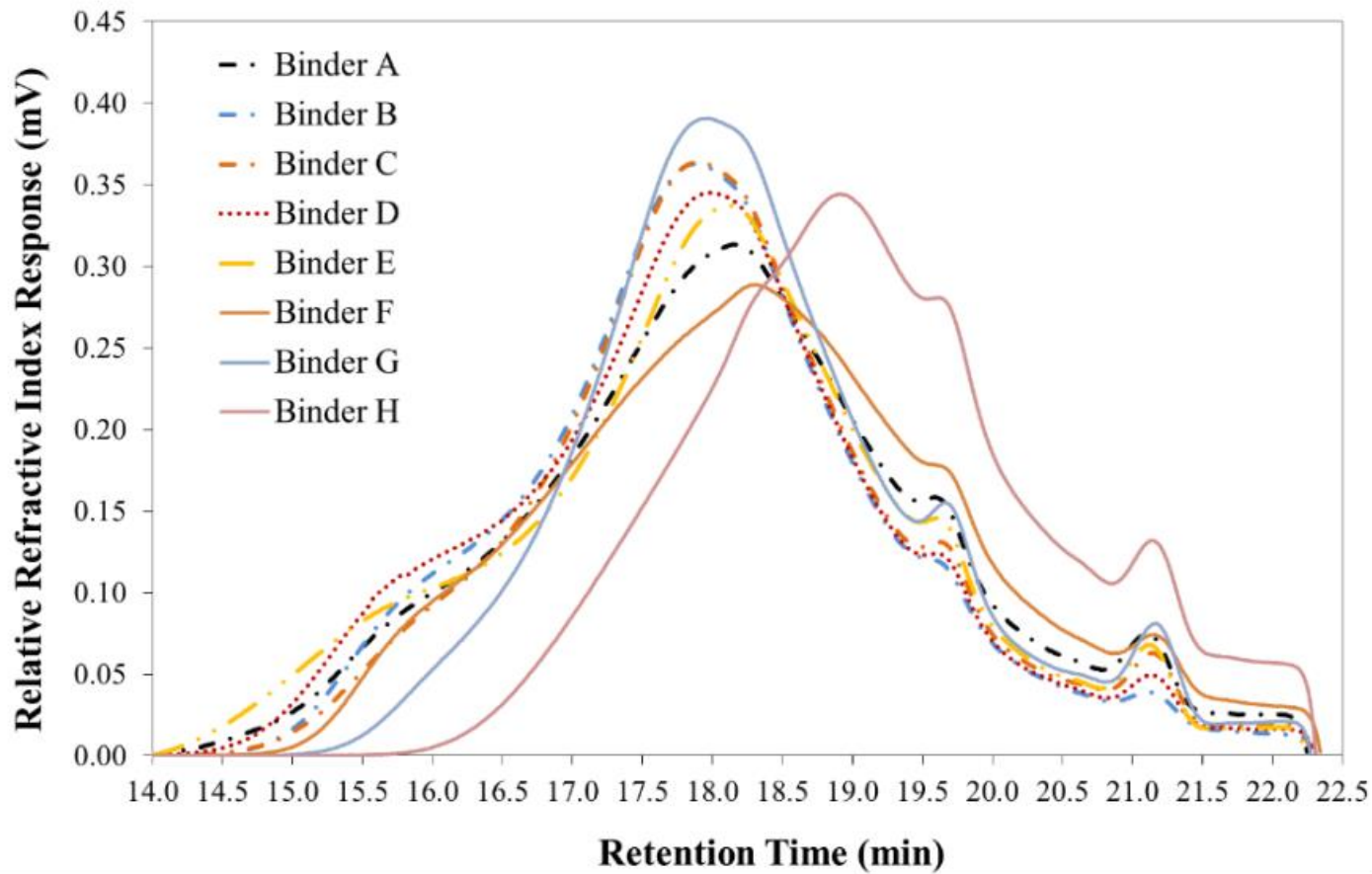
○ Gel particles



GPC spectrum divided into 13 equal elution time areas.

Results

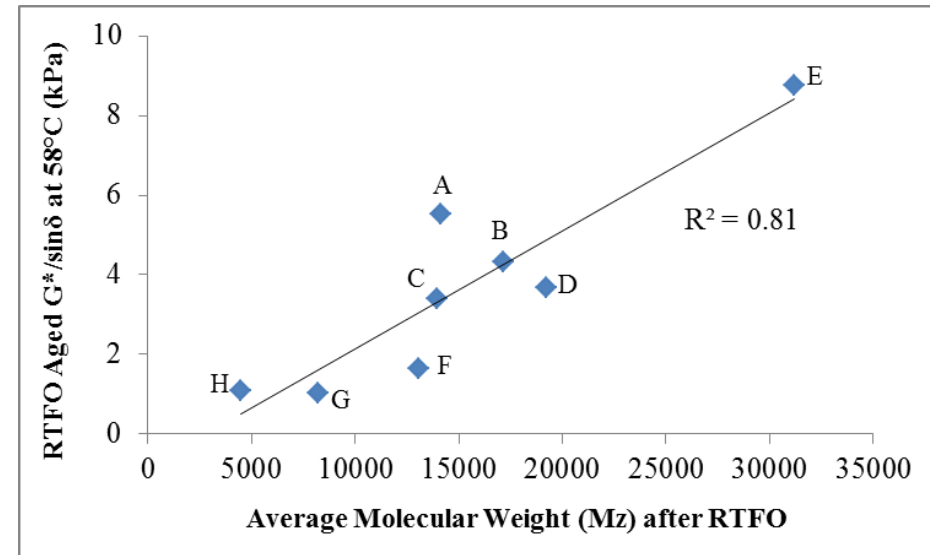
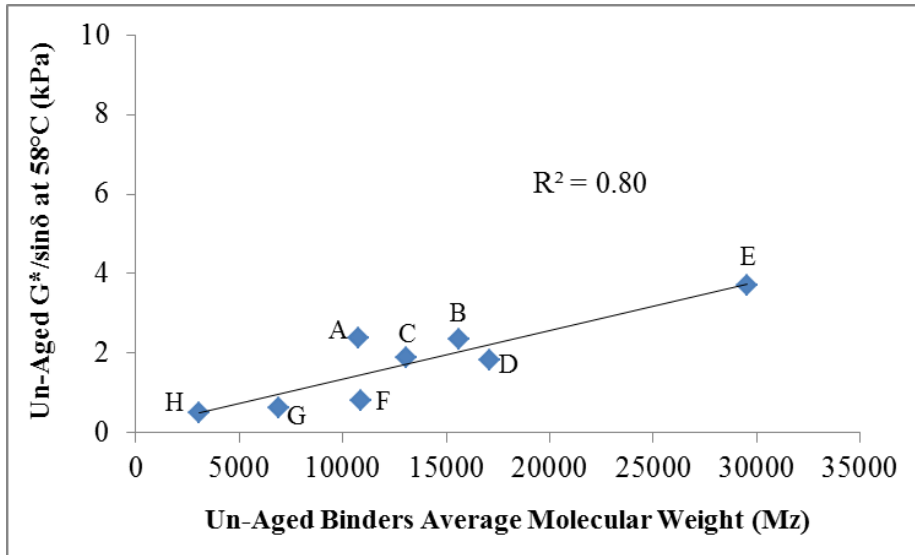
GPC Results



Different patterns of chromatograms and GPC clearly distinct the different molecular size distribution of different binders

Results

Rheological Vs. Chemical Properties-High Temp.

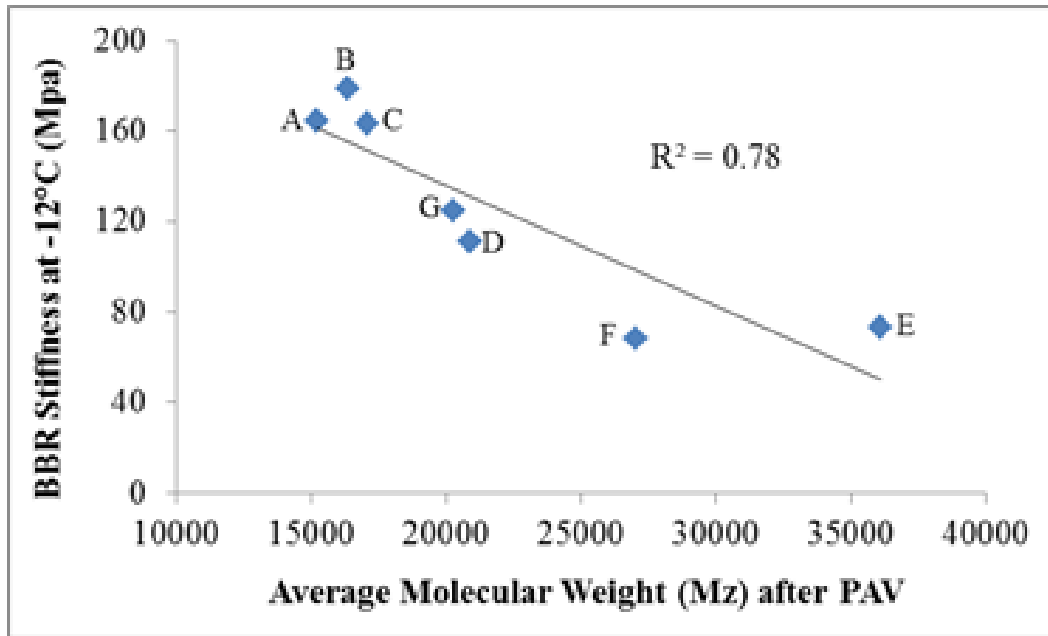


Increase in larger molecules portion of the binder

More asphaltene and higher stiffness at higher temperatures

Results

Rheological Vs. Chemical Properties-Low Temp.



- Relationship between the binder stiffness measured during BBR and the average molecular weight (Mz) in binders
- Decrease Mz corresponds to increments in lighter molecular weight components of the binders

More presence of lighter molecule sizes

Part of maltenes reach their glass transition region at higher temperatures

More brittle behavior

Results

Extended BBR

- Samples were conditioned at their LT+10°C for 72 hours
- BBR testing after 24 hr and 72 hr
- Binders tested in 3 categories based on LT grade:

-12°C

- A
- B
- C

-18°C

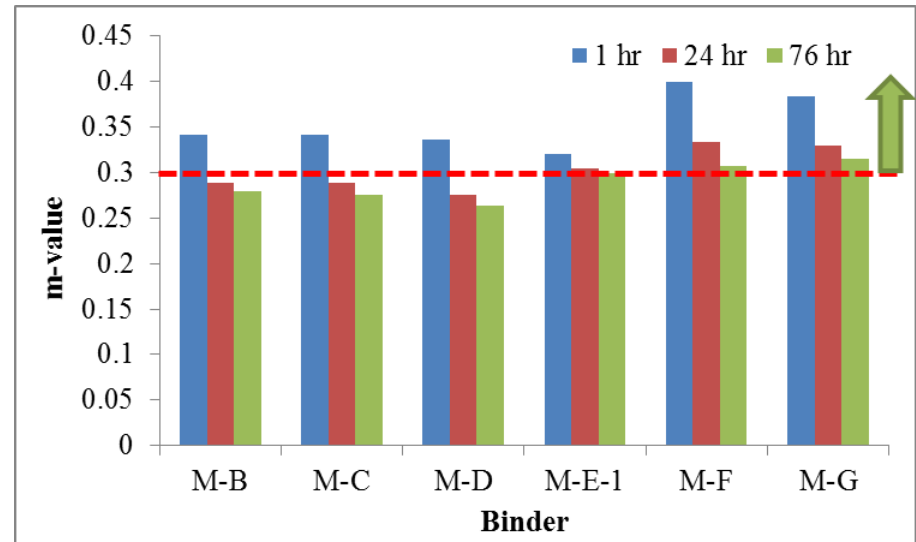
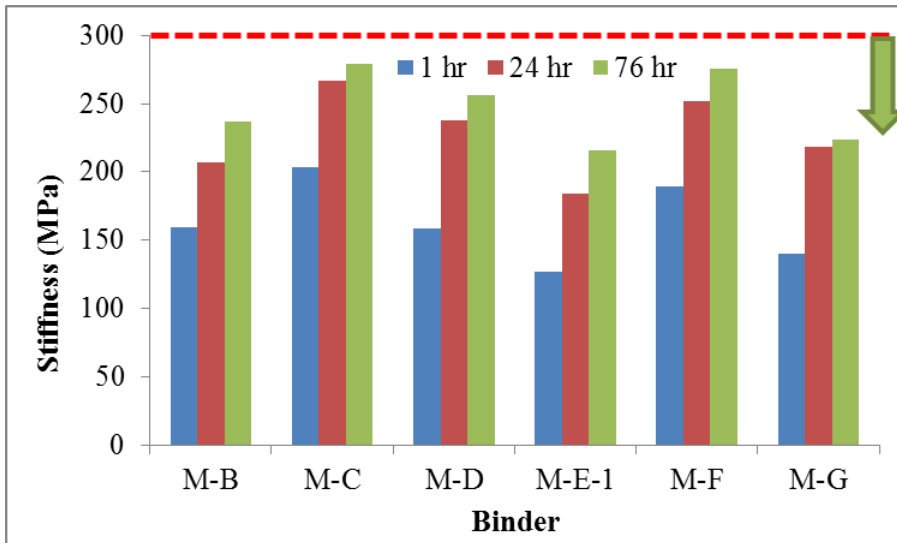
- D
- E
- F
- G
- M-A

-24°C

- M-B
- M-C
- M-D
- M-E-2
- M-F
- M-G

Results

Extended BBR Results @ -24°C



- Overall performance improvement (**less hardening susceptibility**) by using modifications
- Higher polymer content showed to be more effective (**M-F & M-G**)